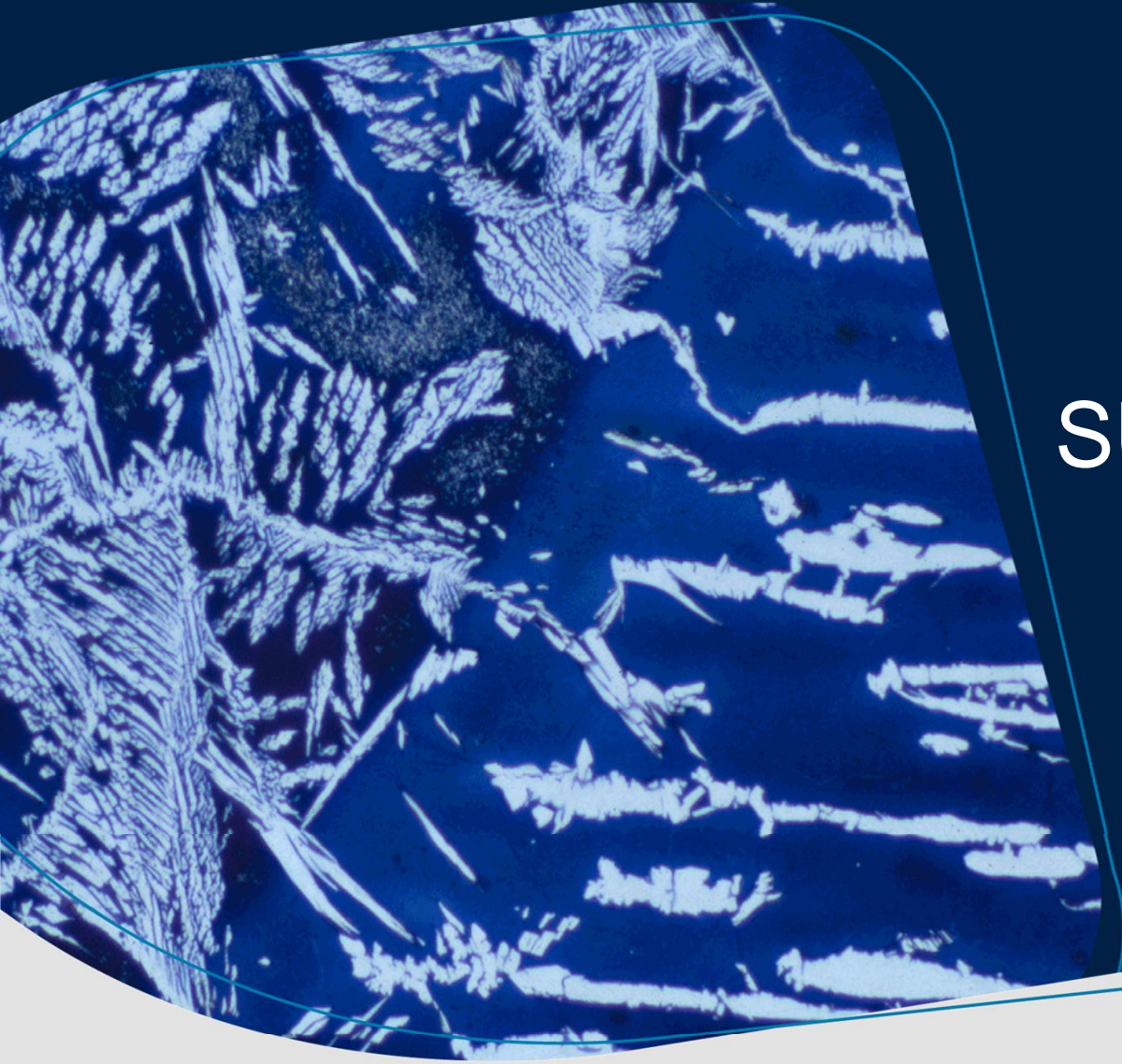




Welding of Duplex & Super Duplex Steels

Advanced – Welding Technology Seminar
Kapfenberg, 23th-26th June 2014





DUPLEX & SUPER DUPLEX

voestalpine Böhler Welding
www.voestalpine.com/welding

voestalpine
EINEN SCHRITT VORAUSS.

Alloying with Cr, Ni, Mo, N, etc.

Increase corrosion resistance and improve properties

ASTM	EN	Grade	Cr	Ni	Mo	N	PRE*	R _{p0.2} **
304L	1.4307	304L	18.1	8.3	-	-	18	200
316L	1.4404	316L	17.2	10.1	2.1	-	24	220
316L	1.4432	316L hi Mo	16.9	10.7	2.6	-	25	220
904L	1.4539	904L	20	25	4.3	-	34	220
S31254	1.4547	254 SMO	20	18	6.1	0.20	43	300
S34565	1.4565	1.4565	24	17	4.5	0.45	46	420
S32101	1.4162	LDX 2101	21.5	1.5	0.3	0.22	26	450
S32304	1.4362	2304	23	4.8	0.3	0.10	26	400
S82441	1.4662	LDX 2404	24	3.6	1.6	0.27	33	480
S32205	1.4462	2205	22	5.7	3.1	0.17	35	460
S32760	1.4501	Zeron 100	25.4	6.9	3.8	0.27	42	530
S32750	1.4410	2507	25	7	4	0.27	43	530

* PRE = %Cr + 3.3x%Mo + 16x%N, ** Hot rolled plate, min values at 20°C according to EN 10088

Fillers for welding standard duplex

Typical composition (wt-%)

	C	Cr	Ni	Mo	N	Mn
Base material LDX 2101[®]	0.03	21.5	1.5	0.3	0.22	5.0
SMAW 3D LDX 2101 3D	0.04	23.5	7.0	0.3	0.14	0.7
FCW LDX 2101-PW	0.03	24.0	9.0	0.4	0.13	0.9
Wire LDX 2101	0.02	23.0	7.0	<0.5	0.14	0.5
Base material 2304	0.02	23.0	4.8	0.3	0.10	-
SMAW 2304 3D	0.02	24.5	9.0	-	0.12	0.8
FCW 2304-PW	0.03	24.0	9.0	0.7	0.14	0.8
Wire 2304	0.02	23.5	7.0	<0.5	0.14	0.5
Base material LDX 2404[™]	0.02	24.0	3.6	1.6	0.27	3.0
SMAW 2404	0.02	24.0	8.5	2.0	0.16	0.7
FCW 2404	0.03	24.5	8.5	1.9	0.16	0.9
Wire 2205	0.02	23.0	8.5	3.1	0.17	1.6
Base material 2205	0.02	22	5.7	3.1	0.17	-
SMAW 2205 3D	0.02	23.0	9.5	3.0	0.15	0.7
FCW 2205-PW	0.03	22.7	9.0	3.2	0.13	0.9
Wire 2205	0.02	23.0	8.5	3.1	0.17	1.6
Base material 2507	0.02	25	7	4	0.27	-
SMAW 2507/P100 3D	0.02	25.5	9.2	3.6	0.24	0.9
FCW 2507/P100	0.02	25.3	9.8	3.7	0.23	0.4
⁴ Wire 2507/P100	0.02	25.0	9.5	4.0	0.25	0.4

Pitting resistance lower for welds

Importance of filler metal and welding procedure

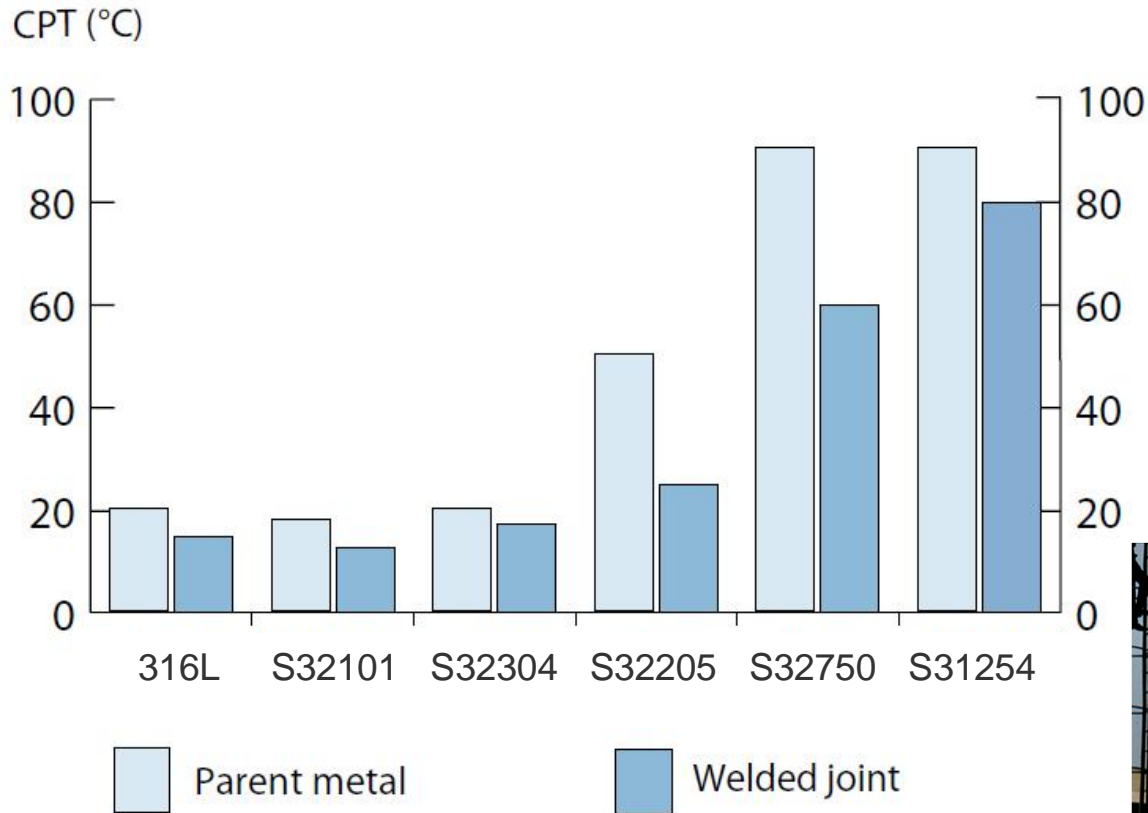
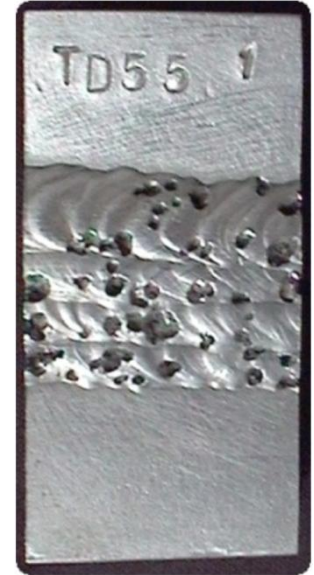
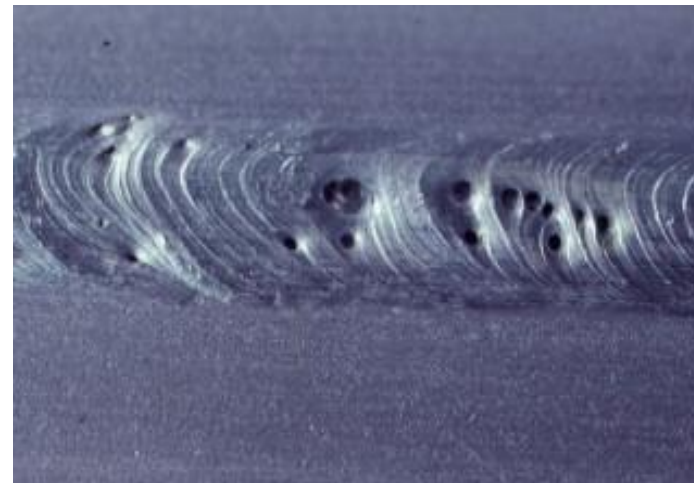


Diagram 1: Typical critical pitting temperatures (CPT) as per ASTM G150 – parent metal and weld, brushed and pickled TIG joint



Effect of welding on corrosion resistance

Welder, welding method and defects



voestalpine Böhler Welding

Post fabrication cleaning

For highest possible corrosion resistance

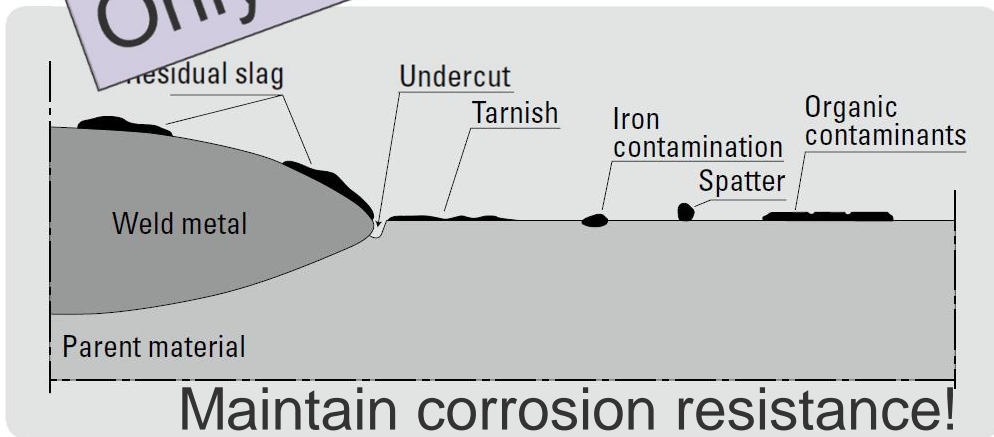
Mechanical methods

- Hand brushing
- Sand blasting
- Grinding
- Polishing

Duplex weld oxide becomes glass-like
Brush welds after cooling



Brushing with steel brush



Cleaning of welds – directly after welding (<math><100^{\circ}\text{C}</math>)

Makes post-weld cleaning easier and shortens pickling time

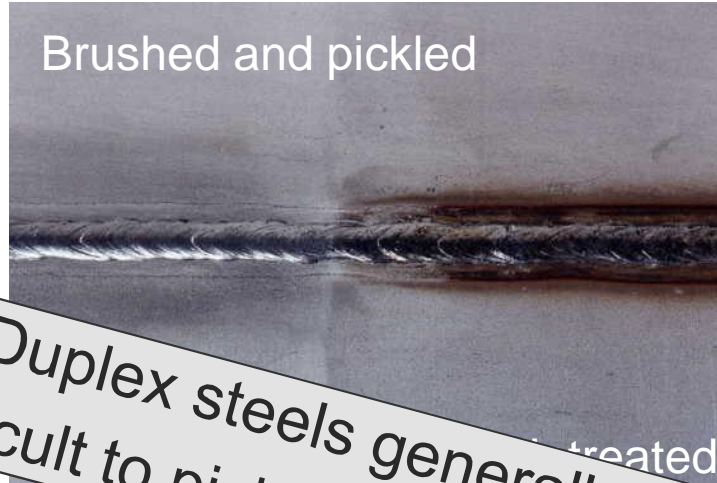


voestalpine Böhler Welding

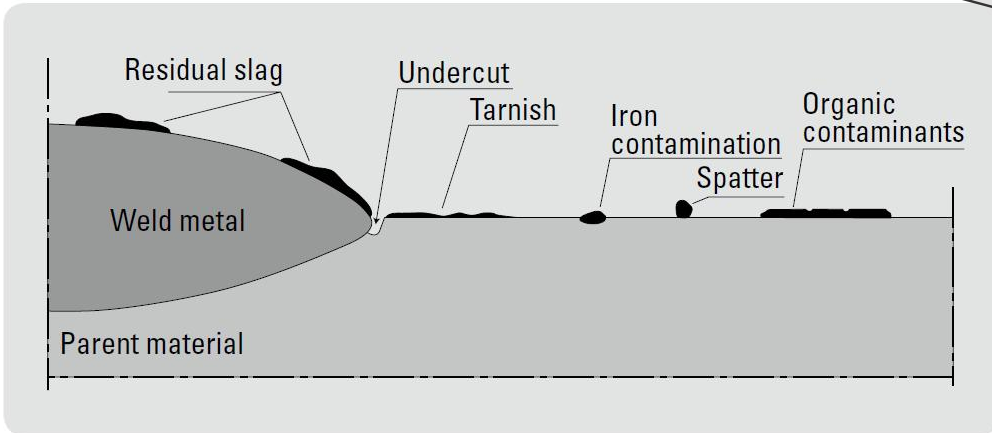
Post fabrication cleaning

Chemical methods – pickling most efficient

- Degreasing
- Pickling
- Passivation



Duplex steels generally more difficult to pickle than 304 and 316



voestalpine Böhler Welding

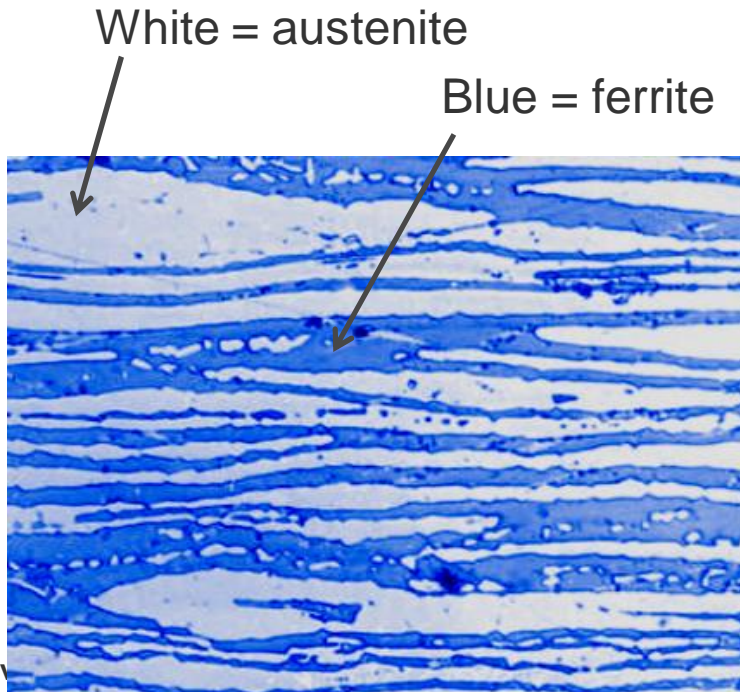


Duplex microstructure

BASE MATERIAL

Controlled cooling

→ 50% ferrite



WELD METAL

Welding method

Base metal composition

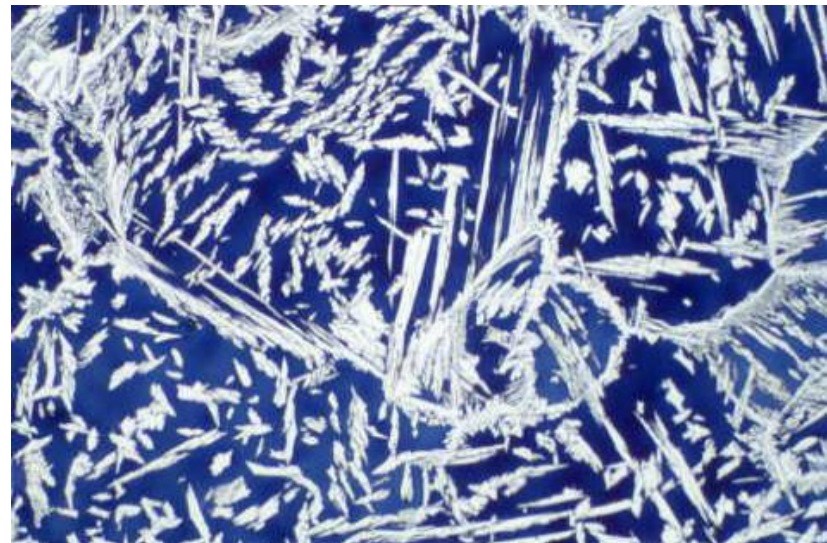
Material thickness / bevelling

Filler metal composition

Shielding / backing gas

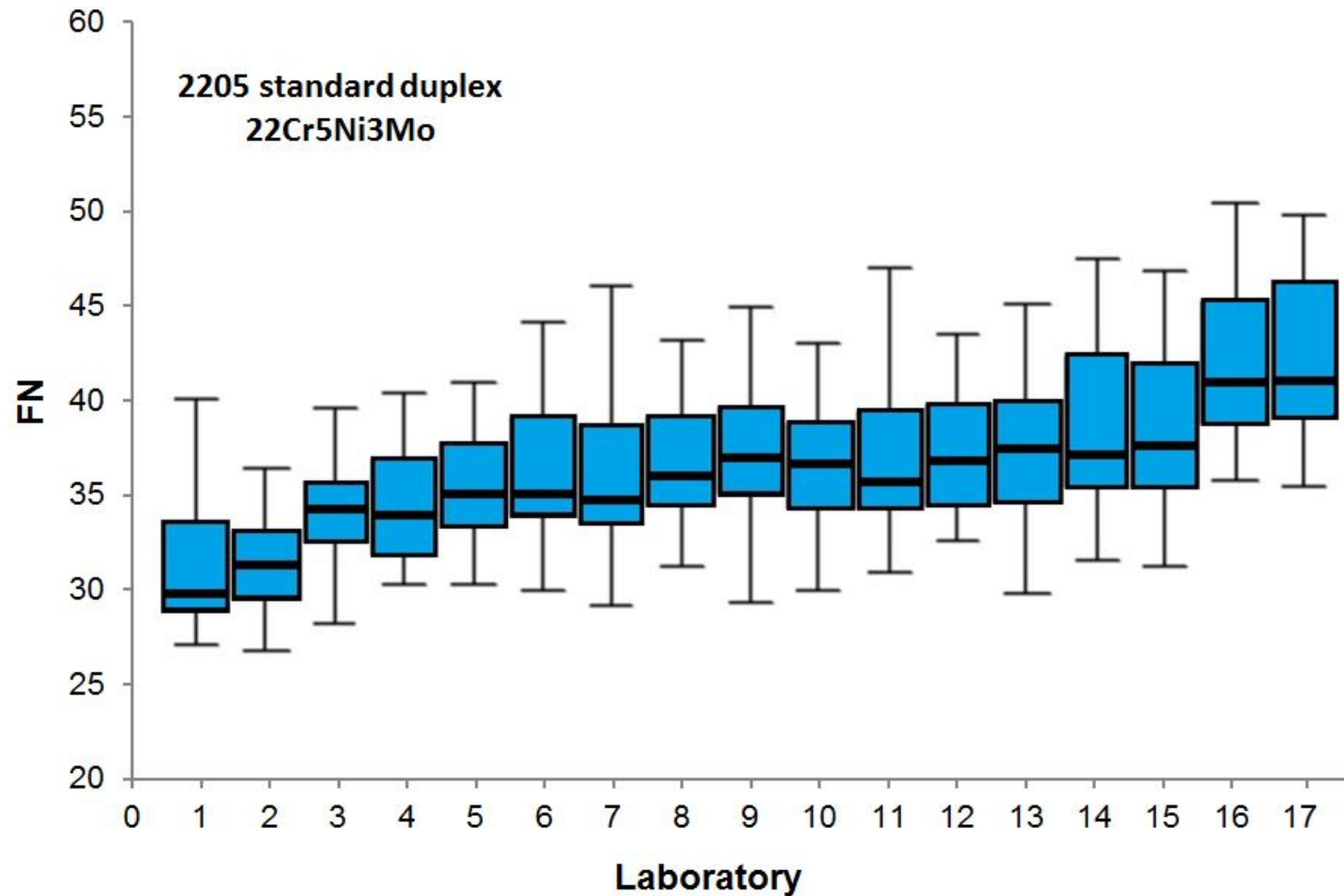
Heat input

Degree of fusion (dilution)



Ferrite measurement varies between labs

IIW round robin test 17 labs



Failure when welding with FCAW 2507/P100-PW

Crack in feeding screw in 12 mm standard duplex 2205



Welding in horizontal position

Welder unsatisfied with visual appearance – GTAW treatment without filler metal

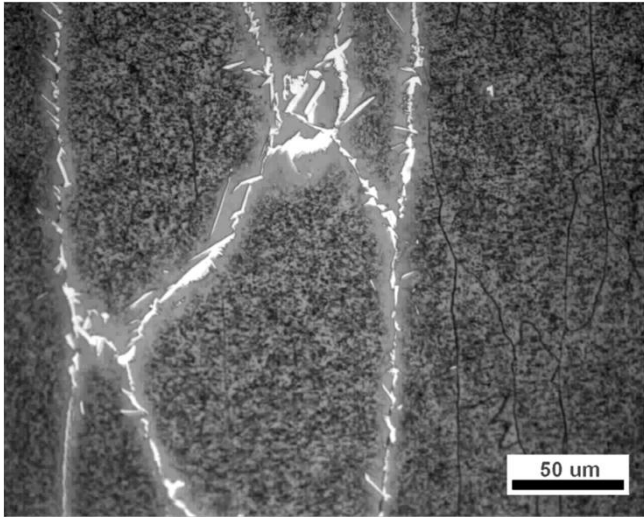
Ferrite content locally 80–90% – brittle weld and cracked after short time in service

On whole feeding screw...

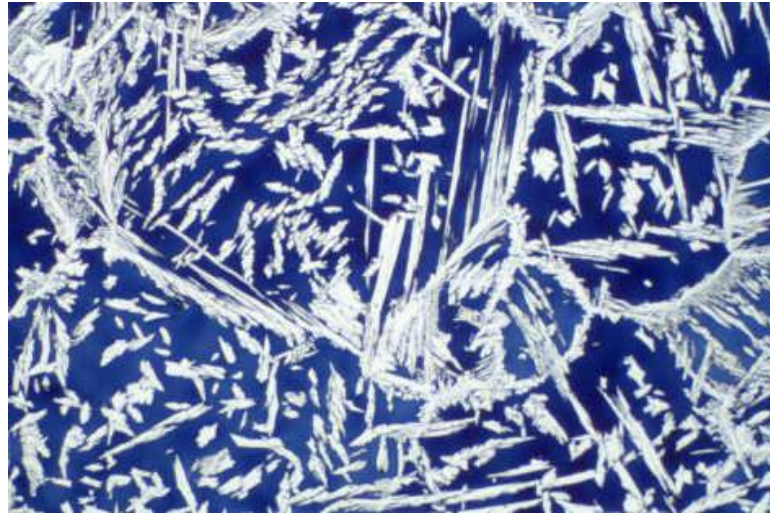
GTAW treatment without filler completely forbidden on duplex constructions

Duplex microstructure after welding

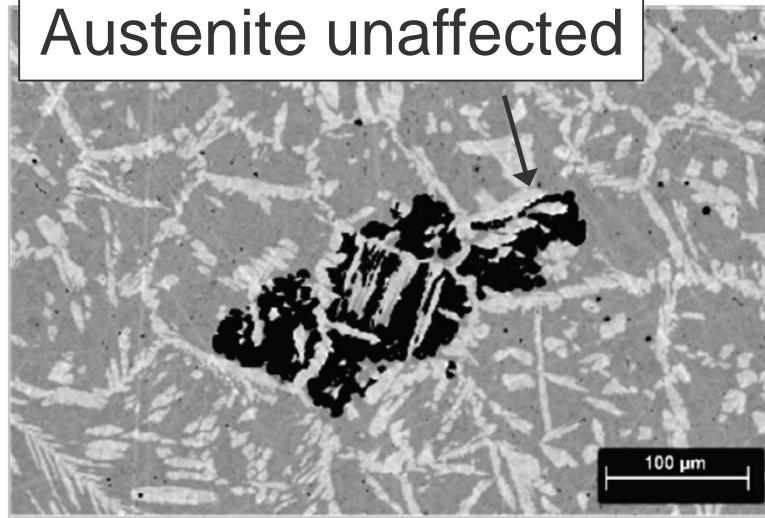
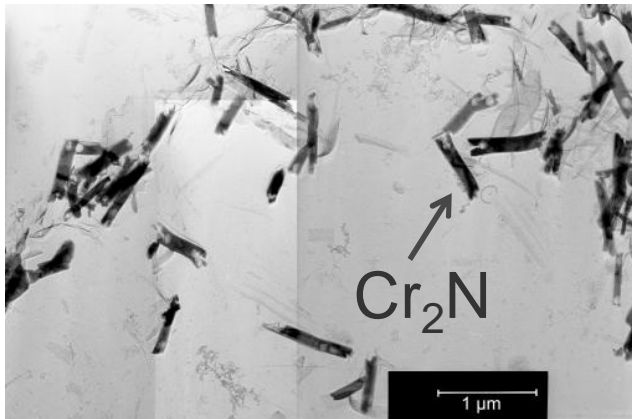
Depends on composition, cooling rate, etc.



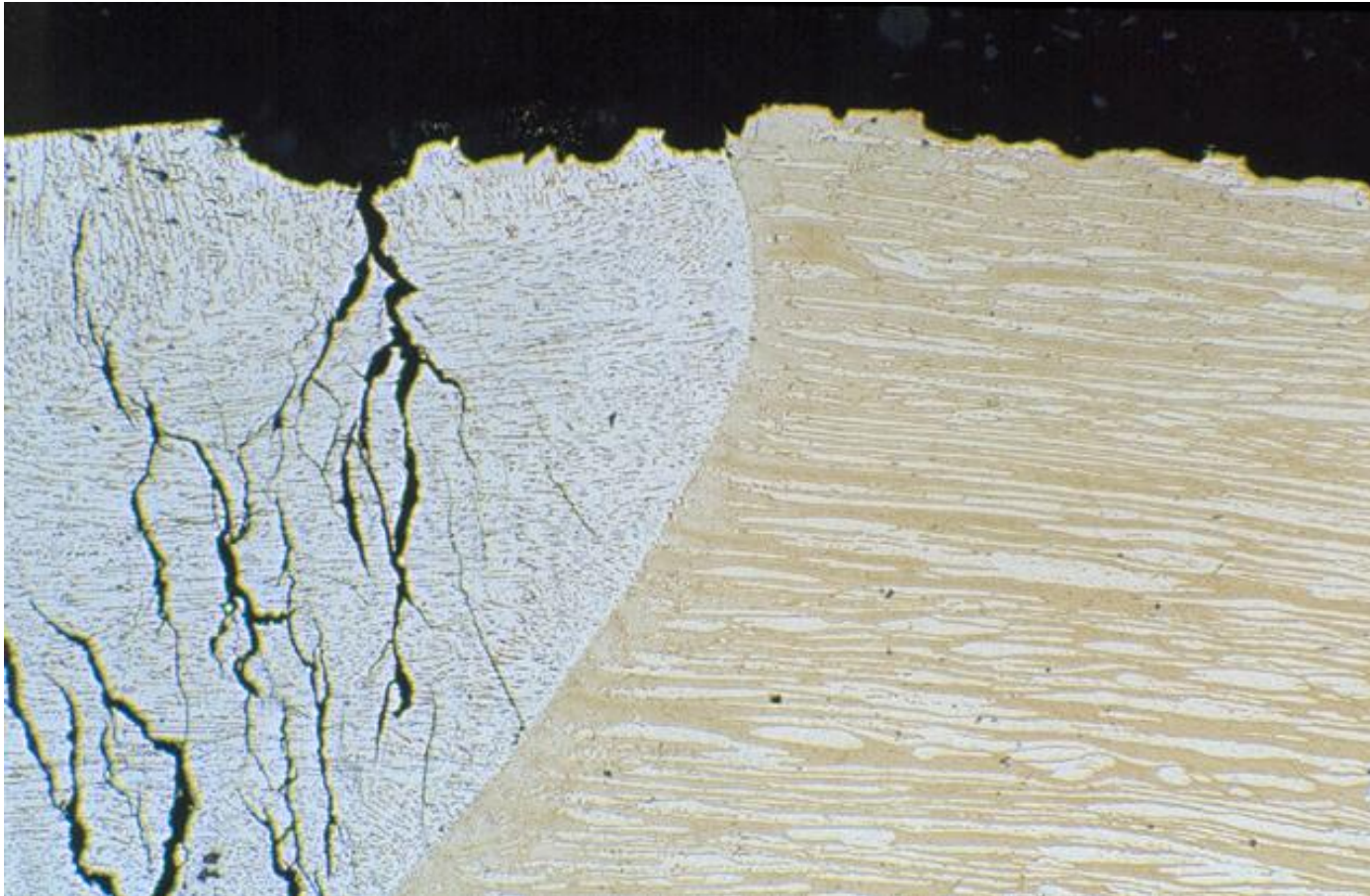
High ferrite without filler



Austenite unaffected



Use of austenitic fillers on standard duplex SCC in 1% NaCl 200°C, 200h with 19Cr19Ni2.5Mo filler



Austenitic weld metal with 10% ferrite - result in SCC in UNS S32205 joints

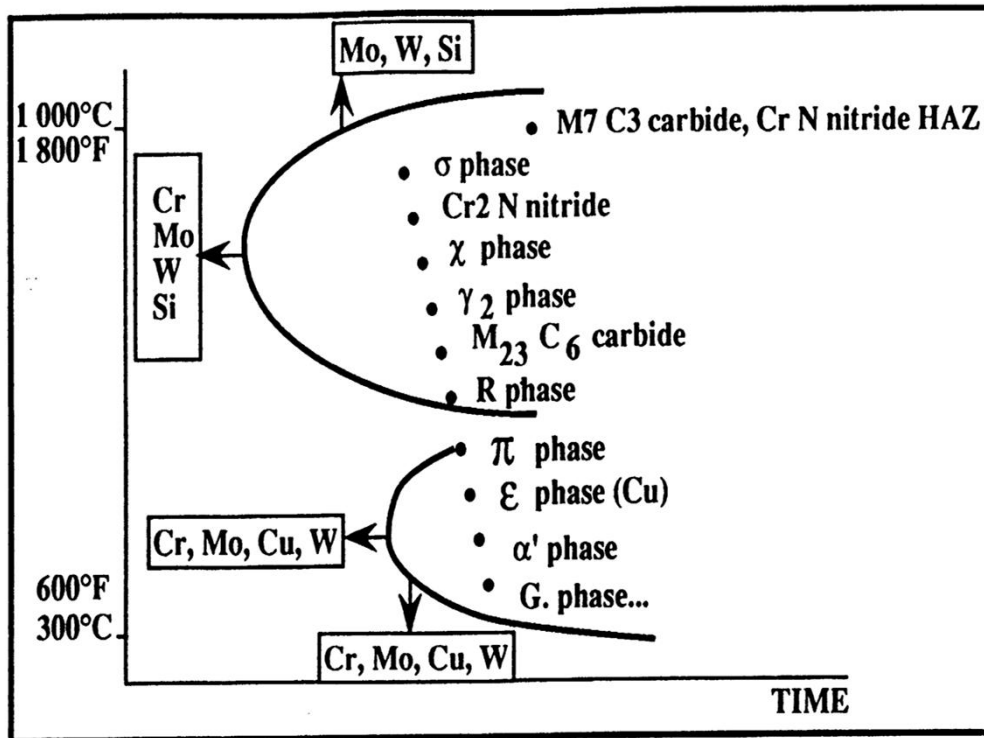
Precipitation of intermetallics (sigma, chi)

Slow cooling rate > 2 kJ/mm

Decreased corrosion resistance and toughness

Alloy and time dependent

Too much energy and time at sensitive temperature



Source: Outokumpu

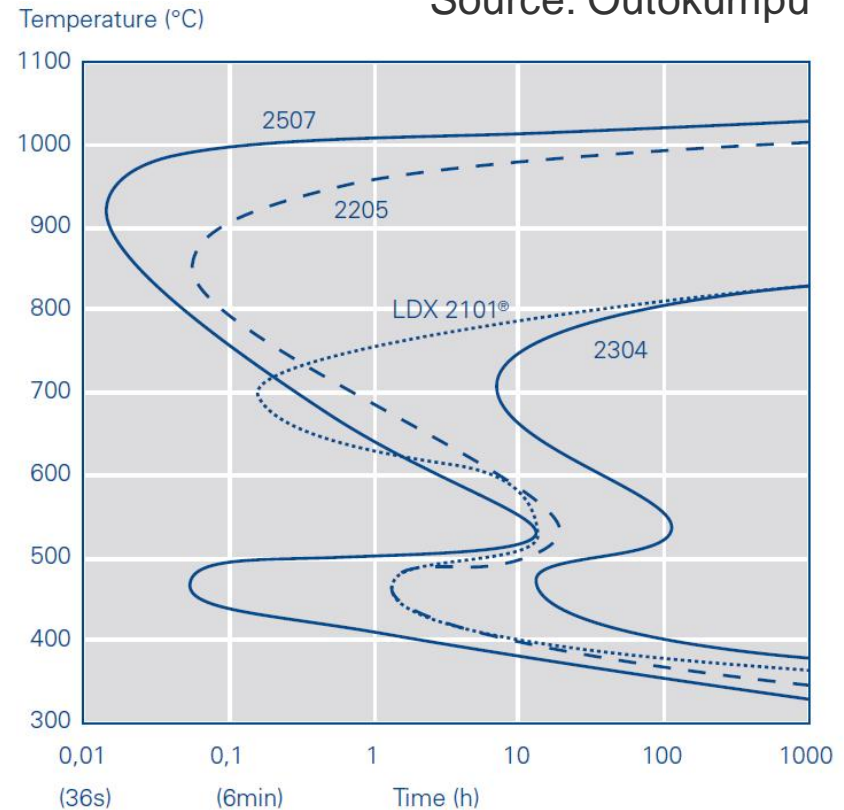


Fig. 1. Curves for reduction of impact toughness to 50% compared to solution annealed condition.

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ONE STEP AHEAD.

Precipitation of intermetallics (sigma, chi)

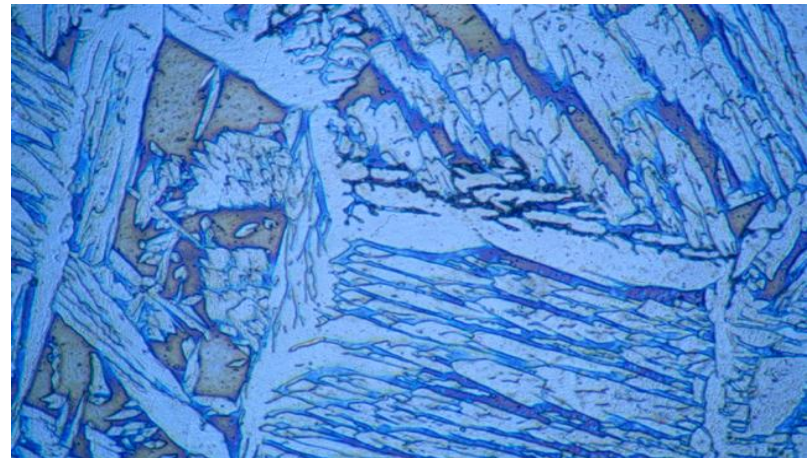
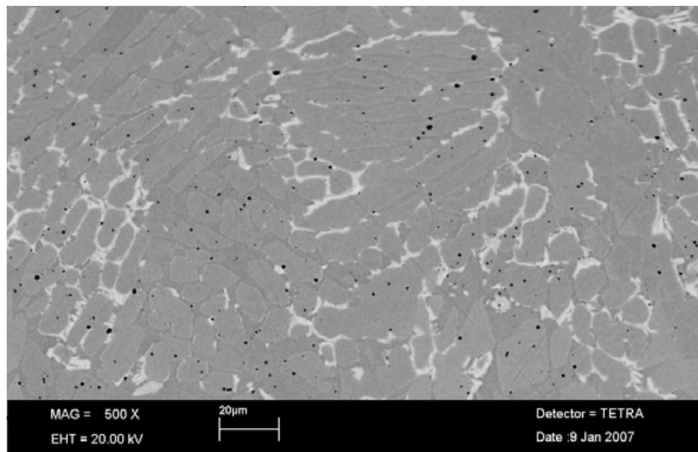
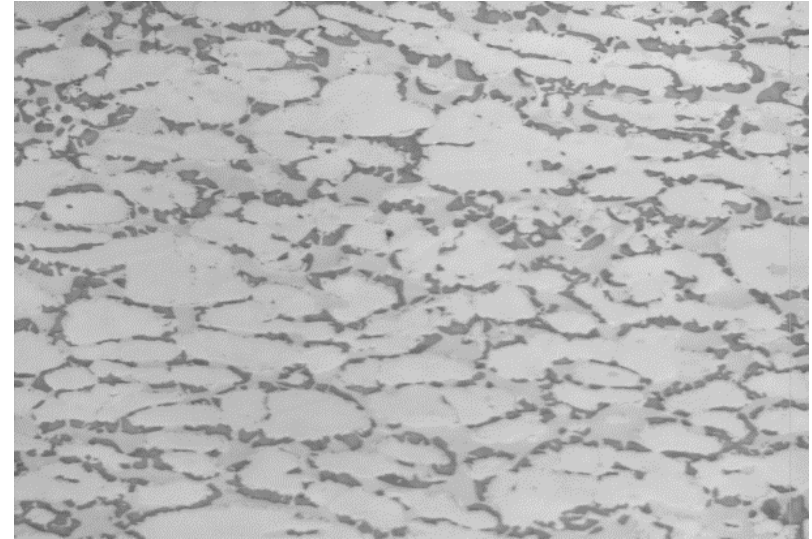
Slow cooling rate > 2 kJ/mm

Specified max heat input
superduplex ≤ 1.5 kJ/mm

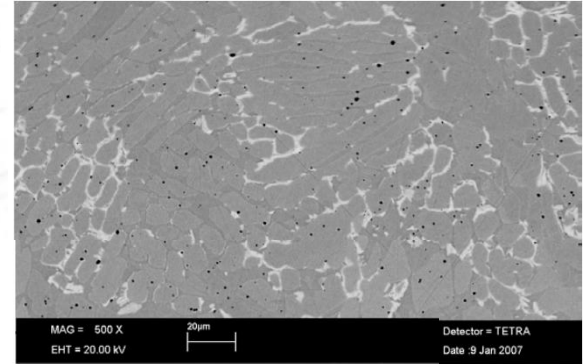
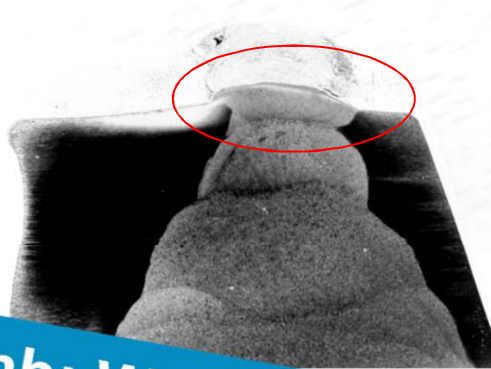
Multipass welding

Interpass (multipass)
temperature 100-150°C

Avoid high heat input in “cold pass”
ito avoid sigma in root bead



Corrosion attack in 25 mm 2507 superduplex H-LO45 position with incorrect welding procedure Pipe system for desalination – TIG (root) and SMAW(rest)

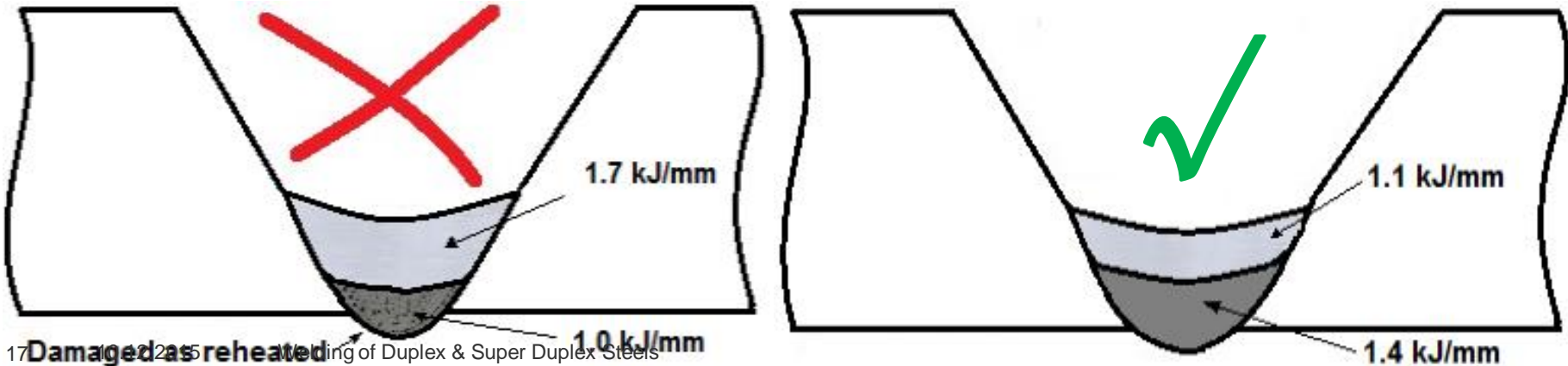


Rule of thumb: Weld cold pass with 70-80% of heat input used for root pass

Root welder

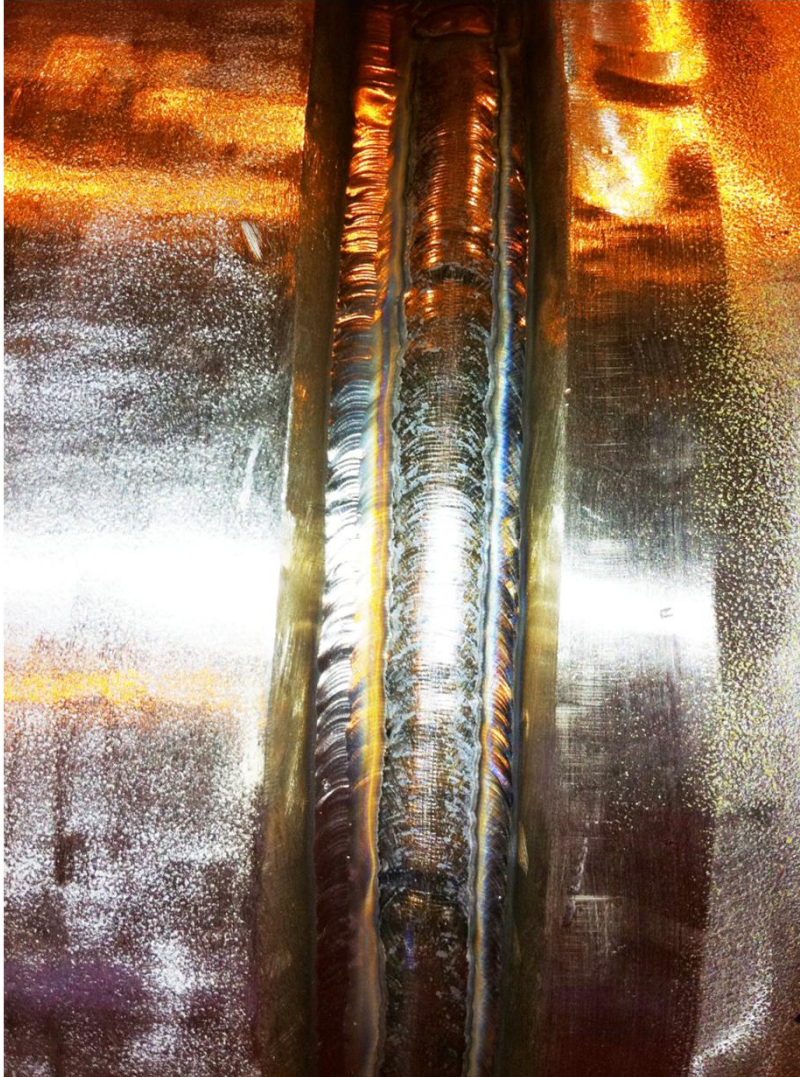
Subsequent welds welded with high

Precipitation of intermetallic phases and decreased corrosion

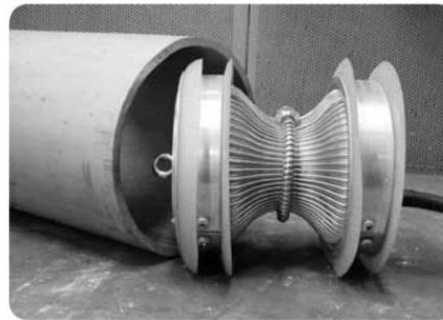
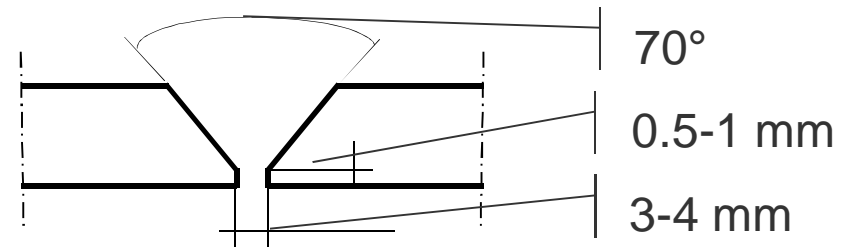


GTAW – most beautiful method

Highest mechanical properties and corrosion resistance



- High quality welds
- Low productivity
- Root and cold passes



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ONE STEP AHEAD.

Domestic water heaters welded with GTAW

Design example EN 13445 at 10 bar, Ø 500 mm and 100°C

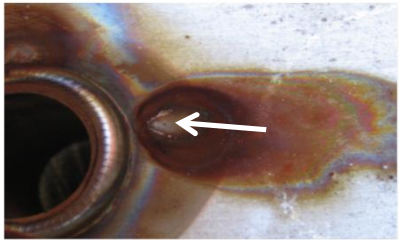
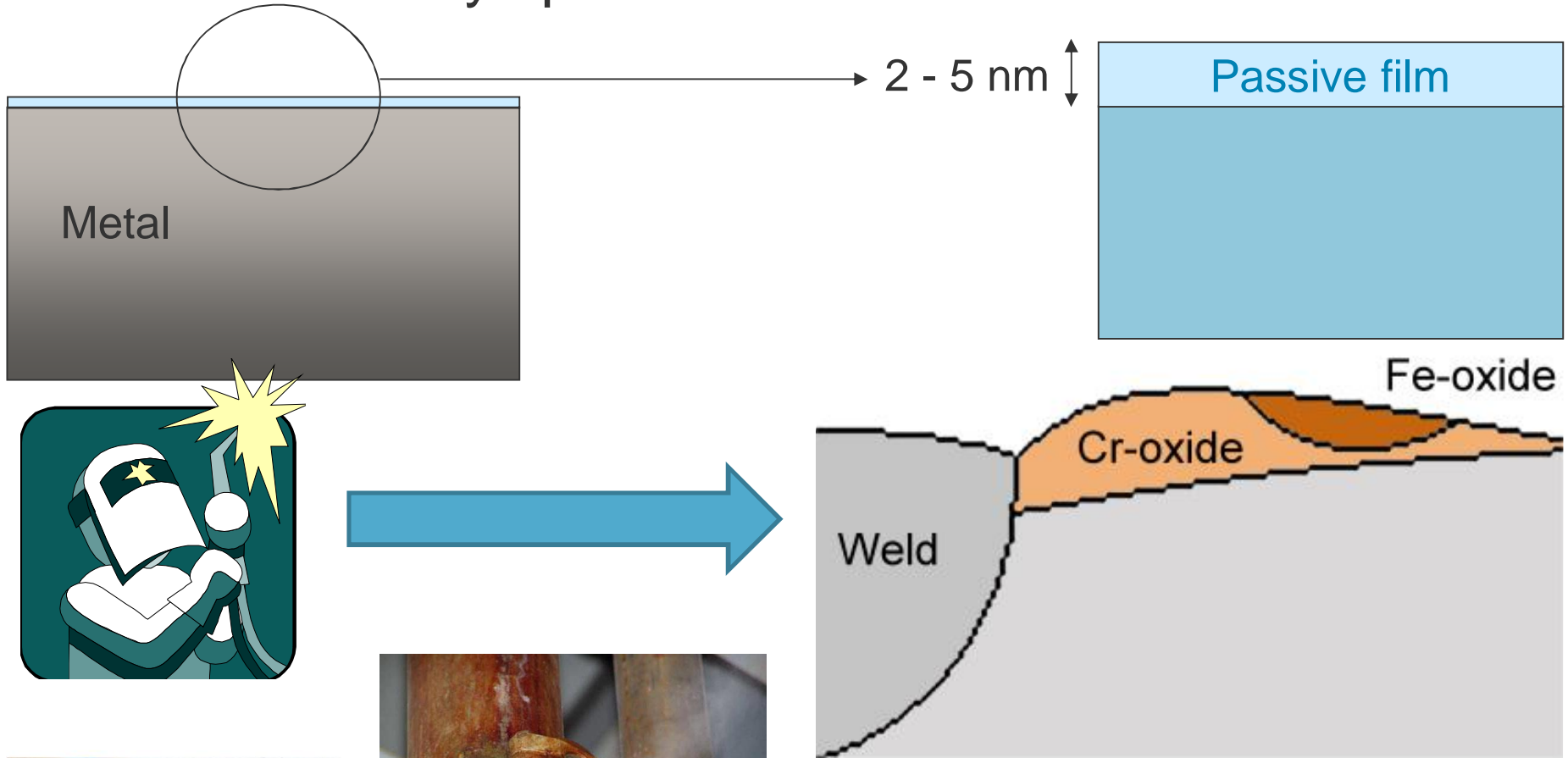
Austenitic 316L	1.8 mm + risk of SCC
Lean duplex LDX 2101	1.0 mm
Lean duplex 2304	1.15 mm
Duplex 2205	1.04 mm
Ferritic 444	1.52 mm

Thin material welded with GTAW
Matching over-alloyed filler metal

Courtesy of Kingspan
Hot Water Systems Ltd



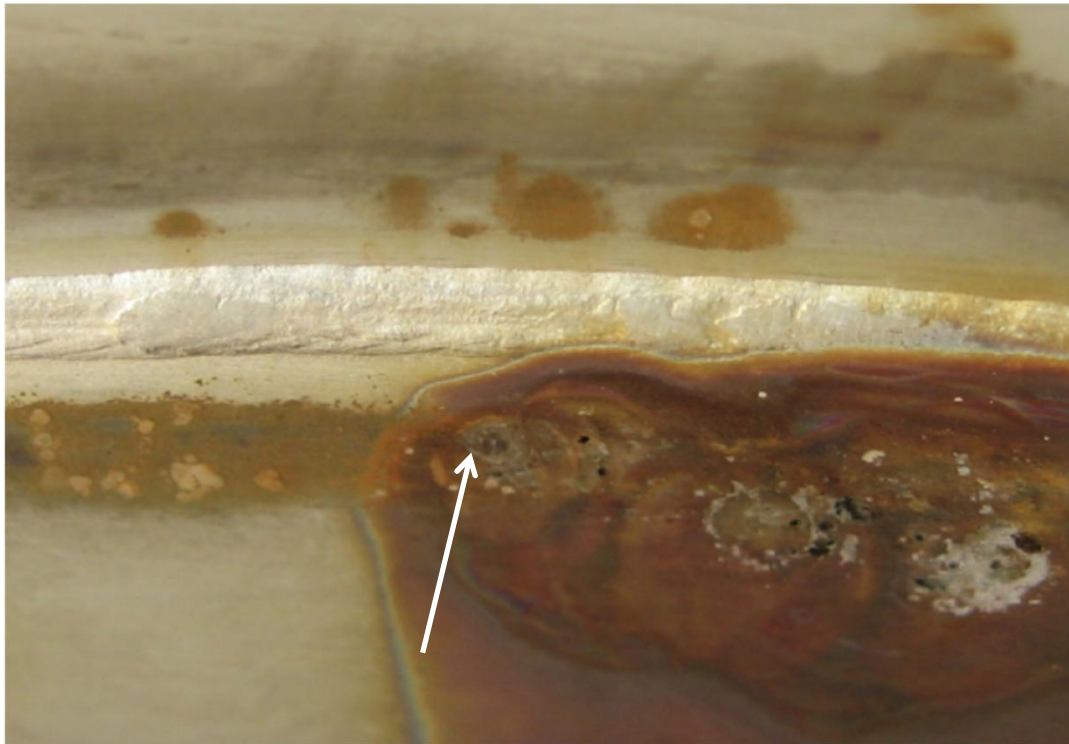
Weld oxide destroys passive film



voestalpine Böhler Welding

Use backing gas – minimize oxygen content

Application with adapters, cardboard or tape

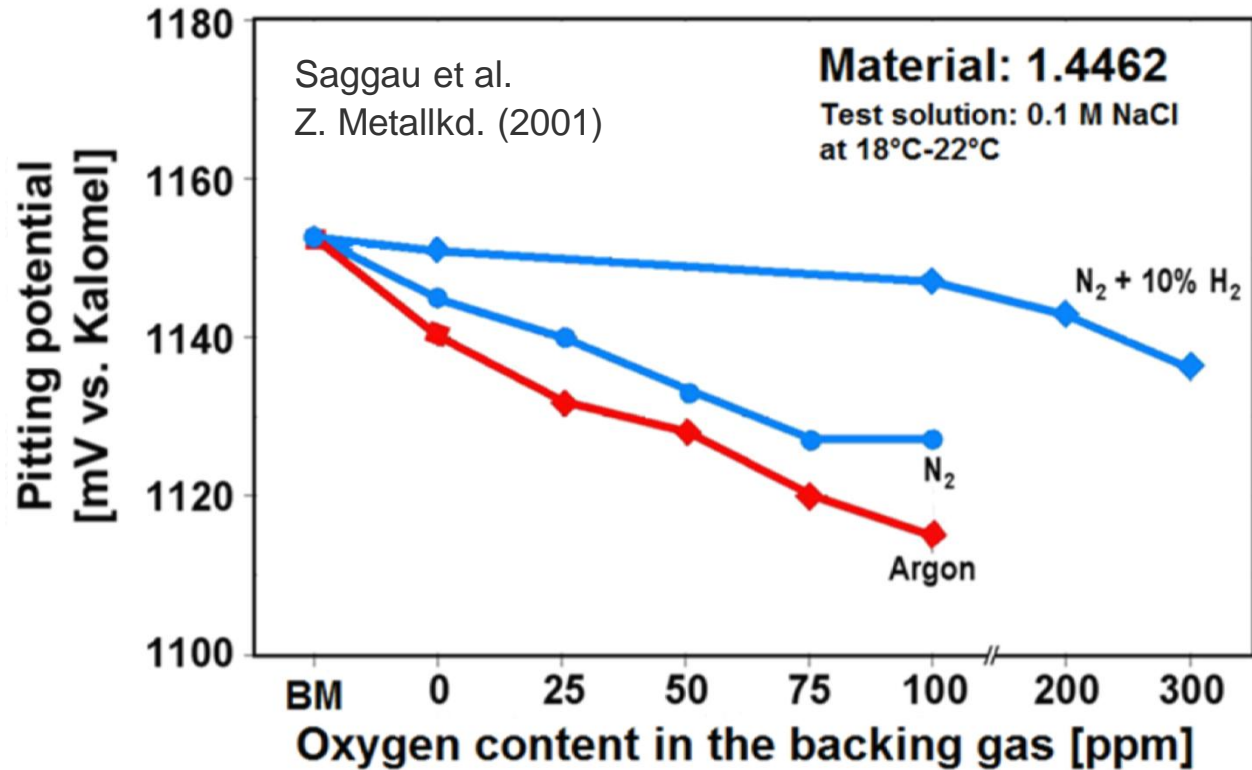


**Corrosion in
Fe-rich oxide**



Effect of oxygen content in backing gas

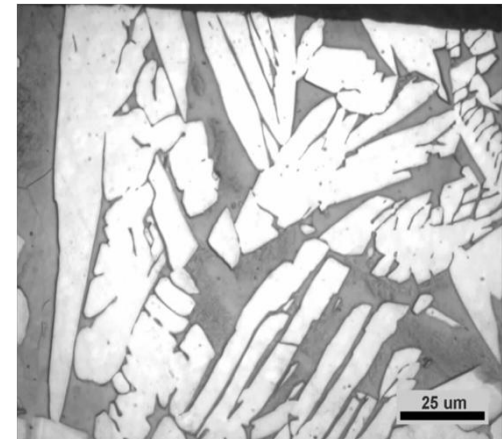
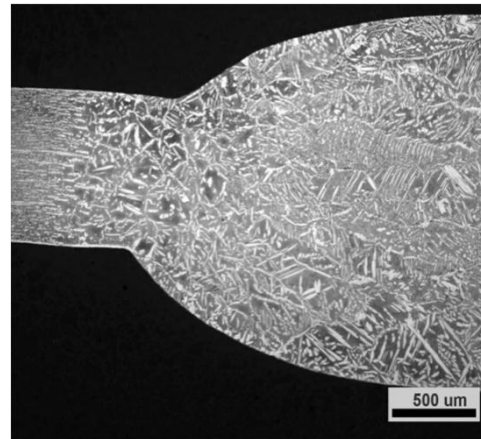
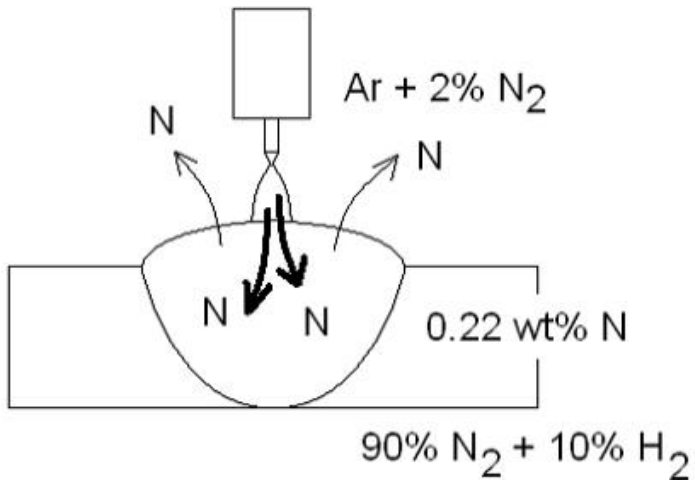
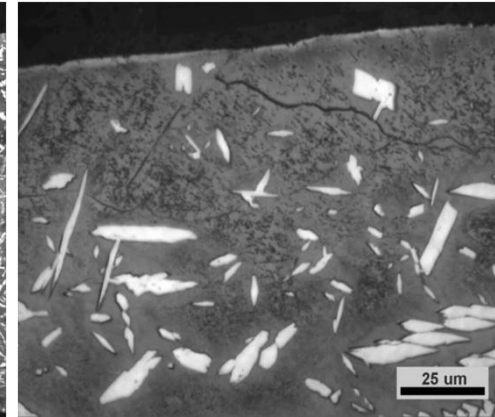
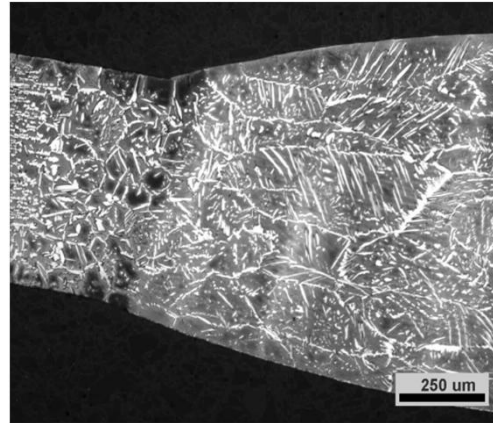
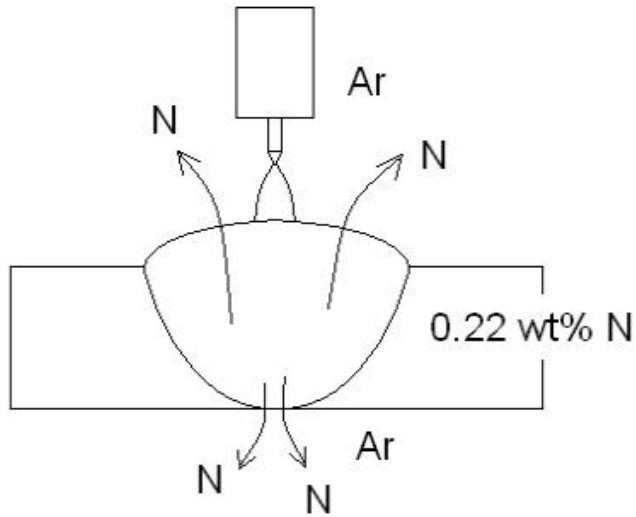
Straw yellow colour normally acceptable ~ 50-60 ppm oxygen



Holmberg and Larén (2001)



Effect of shielding and backing gas (GTAW / TIG)



Lean duplex stainless steel

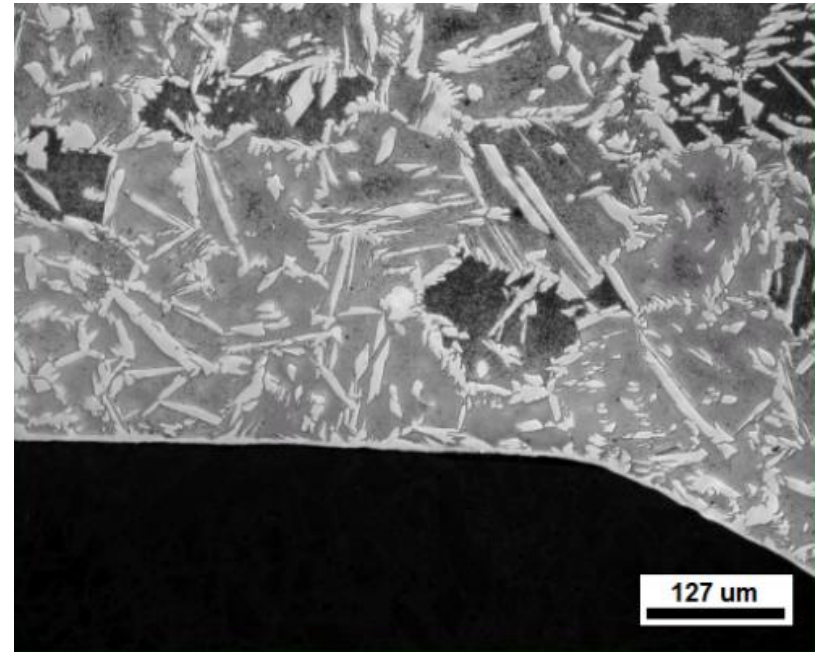
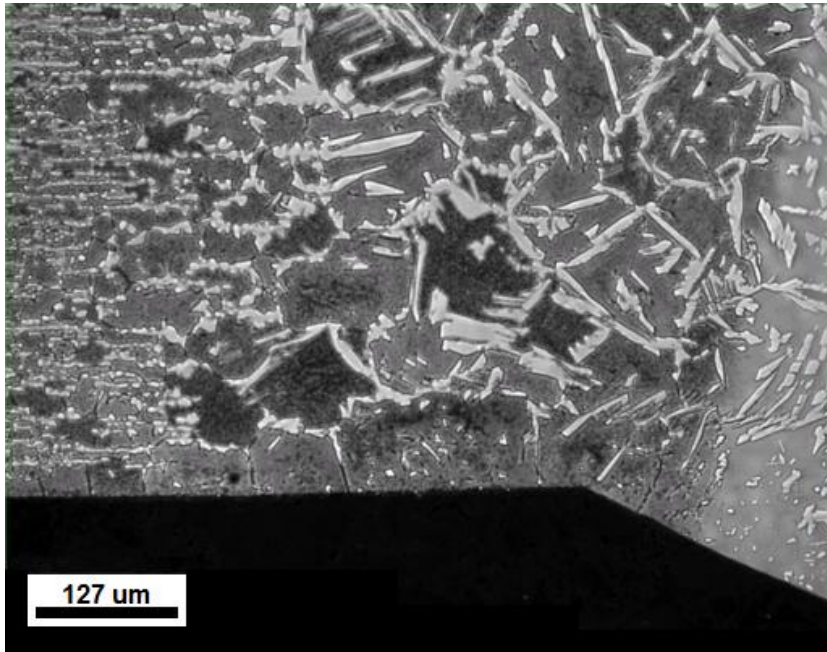
Welded without gap with GTAW method

Pure argon as backing gas

- Nitrogen loss
- High surface ferrite content

90% N₂ + 10% H₂ (N₂ + 0-10% H₂)

- Uniform phase balance
- Protective surface layer of austenite



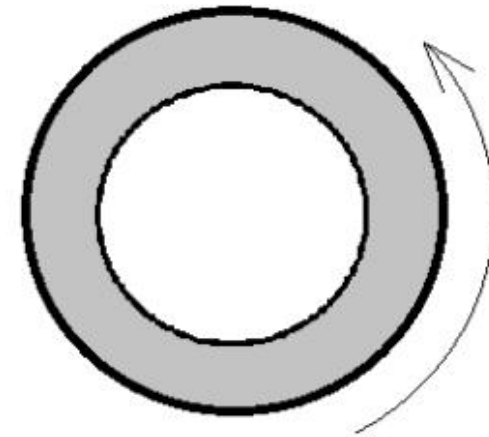
Customer testing – WPS GTAW + FCAW

15 years successful welding of standard duplex

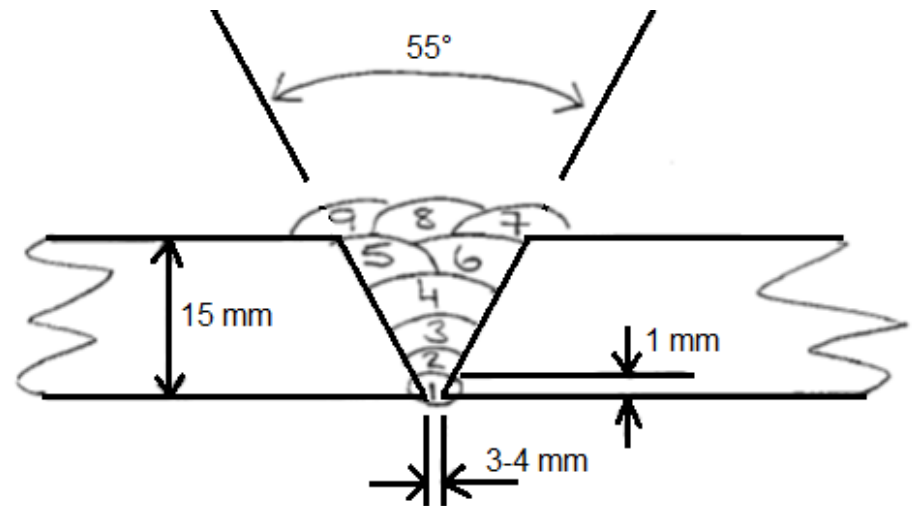
Ø268.6 × 14.27 mm pipe of superduplex UNS S32760
 Zeron 100 GTAW + Avesta 2507/P100-PW NOR FCAW

5G, V joint, interpass temperature max. 100°C

Tensile, bend, hardness, stress corrosion, impact toughness
 test and ferrite content OK



Pass	Method	HI, kJ/mm
1	TIG	1.0
2	TIG	0.6
3	TIG	0.9
4	FCW	1.1
5-9	FCW	0.9-1.5



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ONE STEP AHEAD.

Customer testing – WPS GTAW + FCAW

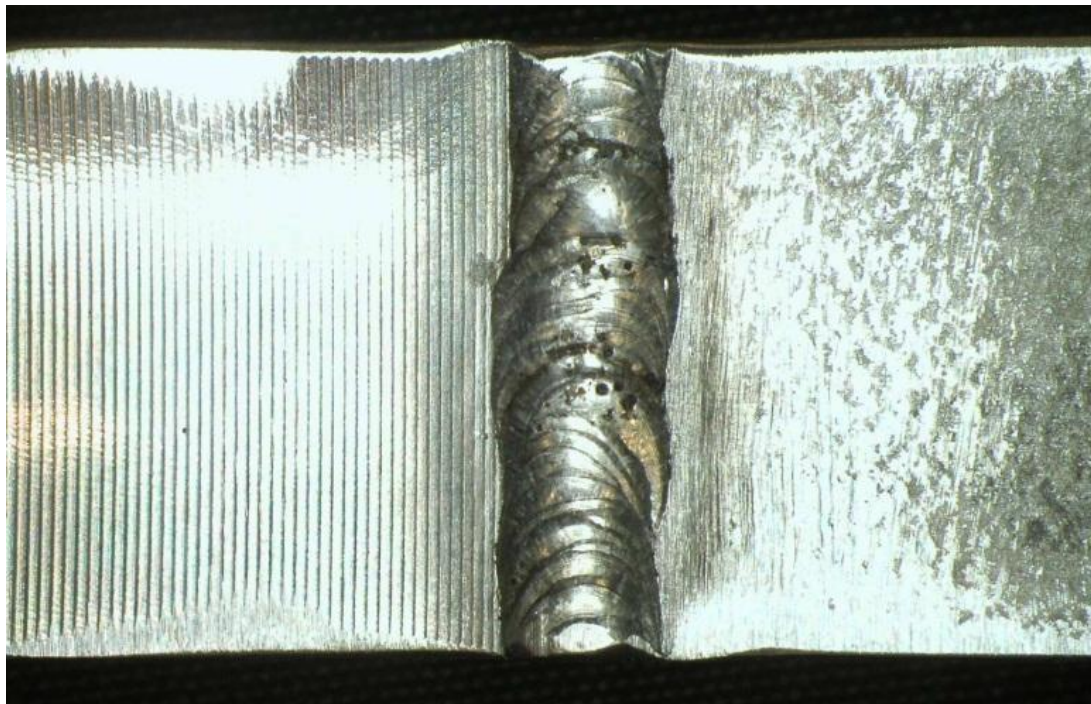
Failed ASTM G48 corrosion test

Pitting attack in GTAW root (not FCAW passes)

Solution to change backing gas from pure argon

Pure nitrogen – no pitting and 3 - 4.01 g/m²

95% N₂ + 5% H₂ (no pitting and 1 - 2 g/m²)



New testing successful
Tensile, hardness, bend,
stress corrosion,
corrosion, impact
toughness and ferrite
content OK

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ONE STEP AHEAD.

Corrosion testing of 7 mm 1.4410 / S32750

H-LO45 GTAW (root) + GTAW (pipe)

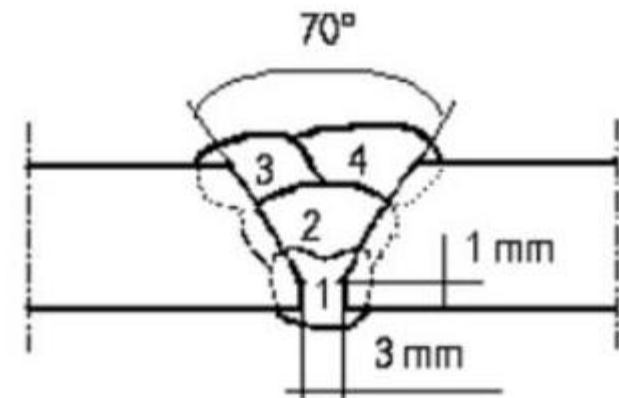
ASTM G48 E – Pickling: 2 h, 40°C, 20% HNO₃ + 5% HF

GTAW – shielding gas Ar + 2% N₂, 2.4 mm Avesta 2507/P100

FCAW – Ar + 18% CO₂ + 0.03% NO, 1.2 mm Avesta 2507/P100-PW

Backing gas 90% N₂ + 10% H₂, interpass temperature < 100°C

Run	Polarity	Current, A	Voltage, V	Speed cm/min	Energy, kJ/mm
1	DC-	87	11.0	2.8-3.8	0.9-1.2
2	DC+	153	24.0	21.5	0.81
3	DC+	156	24.0	28.0	0.64
4	DC+	161	24.3	30.0	0.62



No pitting attack and weight loss << 4 g/m² (0.0000 and 0.5535 g/m²)

Comparison of different backing gases

GTAW 2507 + FCAW Avesta FCW 2507/P100-PW NOR

4 mm root gap, shielding gas 100% Ar / Ar + 18% CO₂

All side bend and tensile testing approved



Backing gas	Average ferrite content, vol.%		
	BM	WM	HAZ
100% Ar	46 ± 2	54 ± 7	66 ± 5
100% N ₂	47 ± 1	44 ± 6	64 ± 3
90% N ₂ + 10% H ₂	47 ± 2	44 ± 9	67 ± 4

Backing gas	Average impact toughness, J	
	20°C	-46°C
100% Ar	67	51
100% N ₂	63	44
90% N ₂ + 10% H ₂	59	43

Backing gas	40°C after pickling	
	Weight loss	Pitting
Ar	5.76	Edge attack
	8.11	Edge attack
N ₂	4.15	
	8.16	
N ₂ /10H ₂	1.05	Edge attack
	2.86	Edge attack

Slag shielded arc welding methods

Covered electrodes – MMA / SMAW

Flexibility – all positions

- Chemical composition

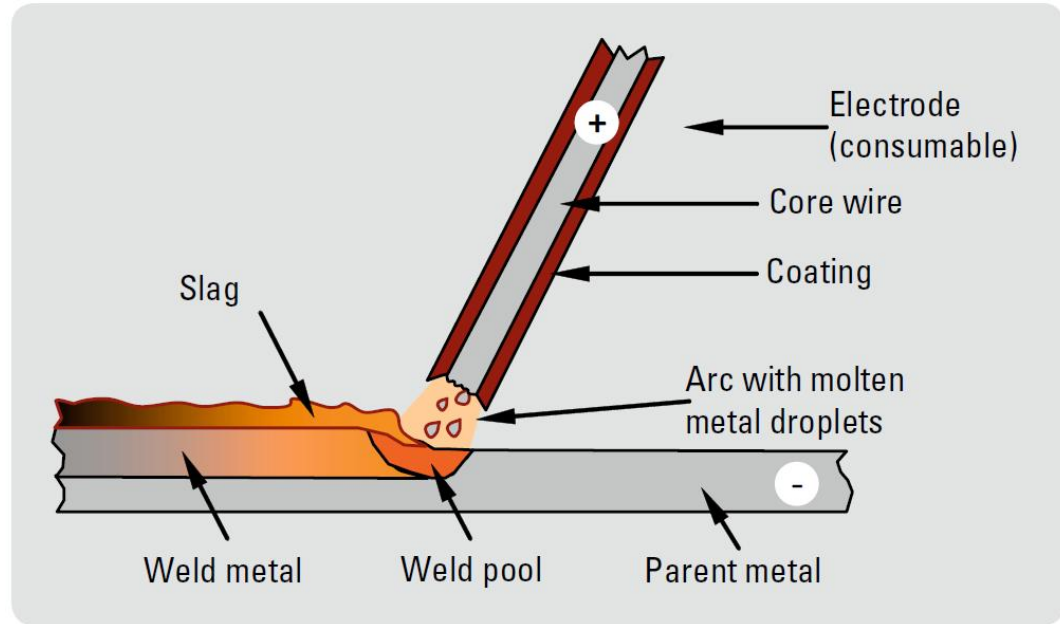
Good weldability

Horizontal and vertical-up position

Material thickness ≥ 2 mm

Suitable for:

- Fabrication welding
- On site welding
- Repair welding



Requires post weld cleaning of root (weld oxide) in drinking water applications!



HP gas cooler for Premier Oil (Indonesia)

6 mm superduplex material S32750

GTAW + SMAW Avesta 2507/P100



P-51, P-52 & P-54 Oil Platforms

Heat exchangers for crude oil for easier pipe transportation, Weight 53 tons. 6.3–50.8 mm superduplex UNS S32750

Filler Metals:	Dimension
Thermanit 25/09 CuT (SMAW)	3.25 + 4.0 mm
Thermanit 25/09 CuT (SAW)	2.40 mm
Marathon 431 (Flux)	Flux
Thermanit 25/09 CuT (GTAW)	2.40 mm



Submerged arc welding SAW – UP

Good weldability – high productivity

Welding thicker materials ≥ 10 mm

Suitable for prefabrication

Penetration less than in standard austenitics

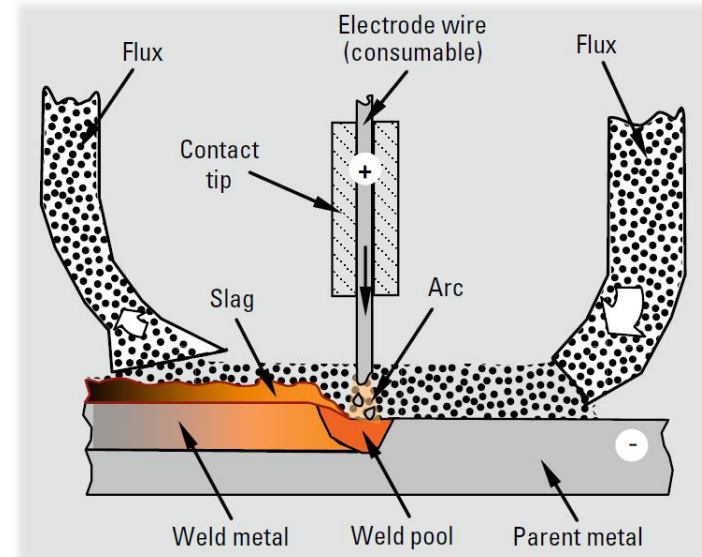
Important with right wire and flux combination

First run(s) can be made with another method

Use basic flux for highest possible impact toughness

Heat input limited in LDX 2101 and 2507

- Avoid big weld pools and high dilution of parent metal
- 2205 & 2304 Heat input up to 3 kJ/mm
- LDX 2101 & 2507/P100 Heat input max 1.0 kJ/mm



Pressure vessel – oil treater & degasser

Fillet welds with $\text{Ø}1.2$ mm Avesta FCW 2507/P100-PW NOR



TIG + SAW for vessel

FCAW for fillet welds

Superduplex base material

NORSOK requirements

40 J impact toughness at -46°C

Alvheim Project

Separator tanks for petrochemical application

Customer: SB Verksted, Drammen, Norway

22% Duplex steel, wall thickness 28 mm

Filler metal: Böhler CN 22/9 PW-FD,
 Thermanit 22/9 UP +
 Flux Marathon 431
 (total weight 3 500 kg)

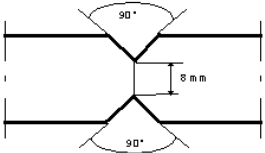
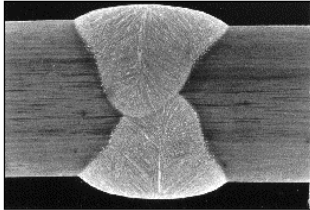
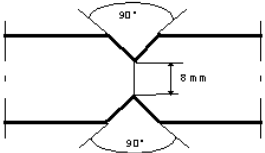
Engineering: Aker Kvaerner Engineering

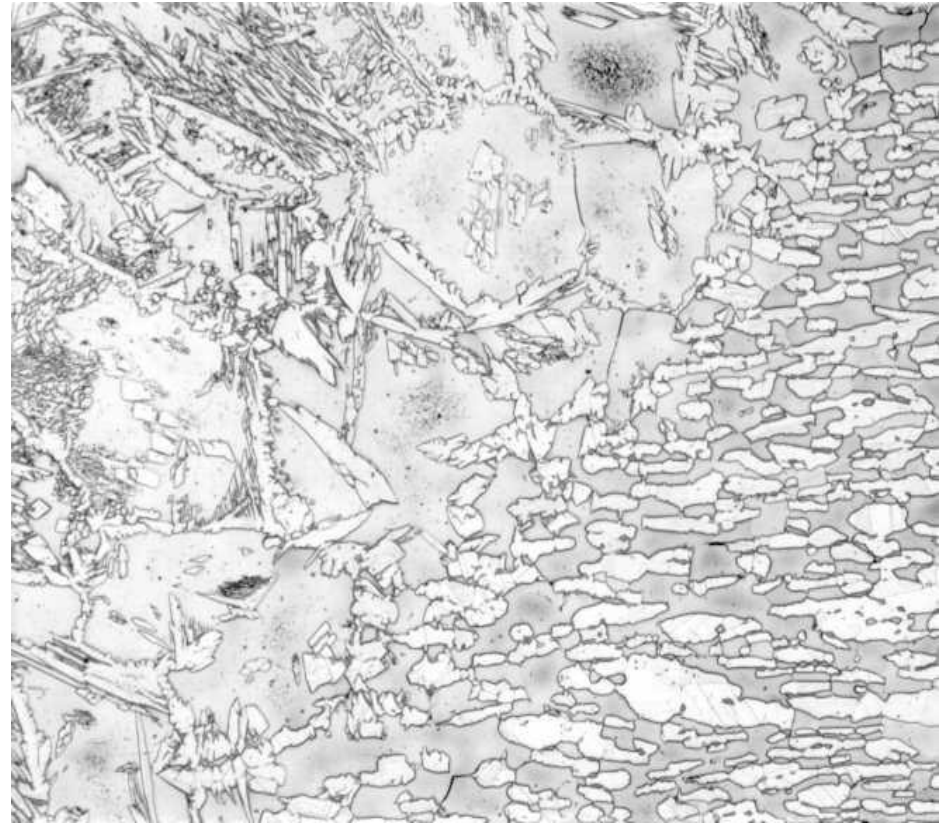
Owner: Marathon Petroleum/Conoco Phillips



Courtesy of SB Verksted

Welding procedures

Avesta Welding		WPAR			WPAR No SAW-1			
		Welded acc. to pWPS: 1			Side:			
Issued by: M. Larén		Charge: M. Larén			Date: 98-07-30			
Base-material: A: 2205 B: 2205		Thickness: 16,5 mm 16,5 mm			Pipe Ø:			
Preheat: °C Interpass temp.: <150°C PWHT: °C		Backing: No grinding of backside.						
Welding position: 1G (PA)		 						
								
Thickness: 16.5 mm Root face: 8 mm Joint angle: 80°		Notes: Drag angle 15° towards travel direction (backhand).						
Run:	Process:	Filler material:	Dia:	Batch No:	Gas/Flux:			
1-2	SAW	2205	3.20 mm	0322	AVESTA 805 Lot 2779			
Run:	Polarity:	Current:	Voltage:	Speed:	Energy:	Stick out:	Wire feed:	Note:
1	DC+	635	32,5	50	2,48	20 mm		
2	DC+	635	32,5	50	2,48	20 mm		
Chemical analysis (Pure weld metal)								
C:	Si:	Mn:	P:	S:	Cr:	Ni:	Mo:	N and Cu:
0,016	0,51	1,44	0,016	0,001	22,7	8,65	3,05	0,17/0,10
Tensile test		Impact test			Bend test:			
Rp0.2:	Rm:	As (%)	Notch:	Temp:	Joule:	Average:	Mandrell dia:	3xT
507 Mpa	716 Mpa	29	KV	+20 °C	198,184,173	185	Root, Cap, Side:	OK
495 Mpa	694 Mpa	30	KV	-40 °C	63,58,68	63		
Corrosion test		Result:			Preparation:			
Type:	Temp:	Weight loss:			(Pickling, brushing, As welded)			
ASTM G48-A	27.5°C 30°C	No attacks. Attack in weld: 0.0012 g			Pickling+brushing			
X-ray:	Grade 5 Aa	Note: Some small porosity						
Liquid penetrant: None		Note:						
Micrographic examination								
		ASTM E562		Ferrite scope MP-3				
Ferrite content:	1.	54.7%		51.4%				
(weld metal)	2.	54.0%		50.6%				
Note:		See report No.: LR 222/98						



Establish proper welding procedure and follow it!

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ONE STEP AHEAD.

Gas shielded arc welding – MIG / MAG – GMAW

Fluidity and arc stability lower than standard
austenitic fillers (spatter)

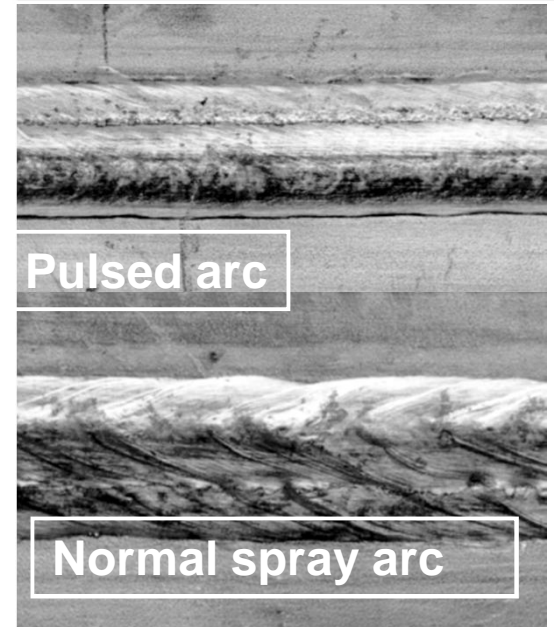
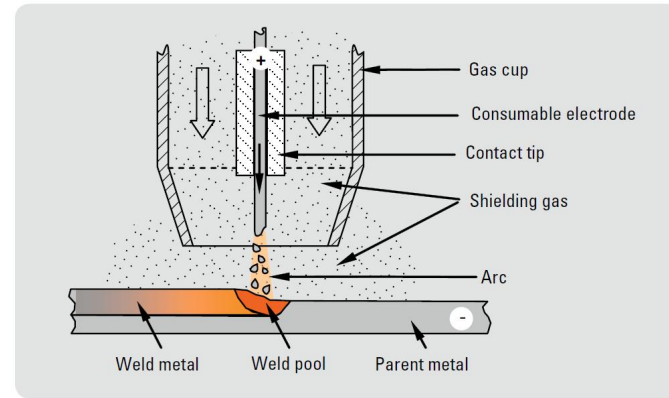
Best results with synergic pulsing

Recommended shielding gas

- Ar + 30% He + 1-3% CO₂
- Ar + 2% O₂ or Ar + 2-3% CO₂

High BM nitrogen content increases sensitivity to
porosity – superduplex pure argon

FCAW an alternative (less pores)



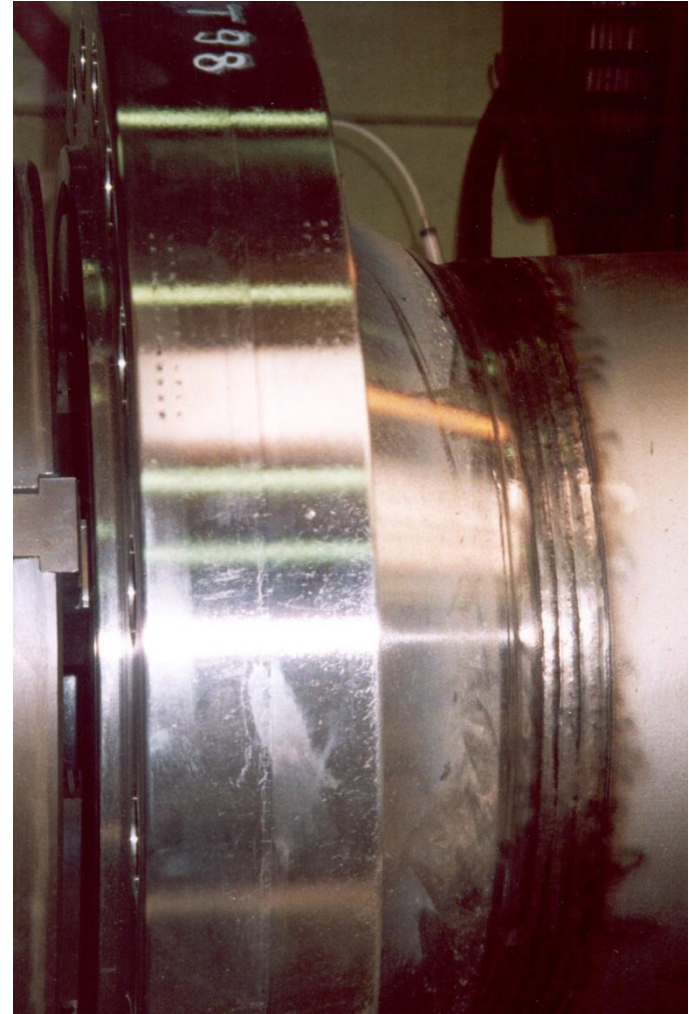
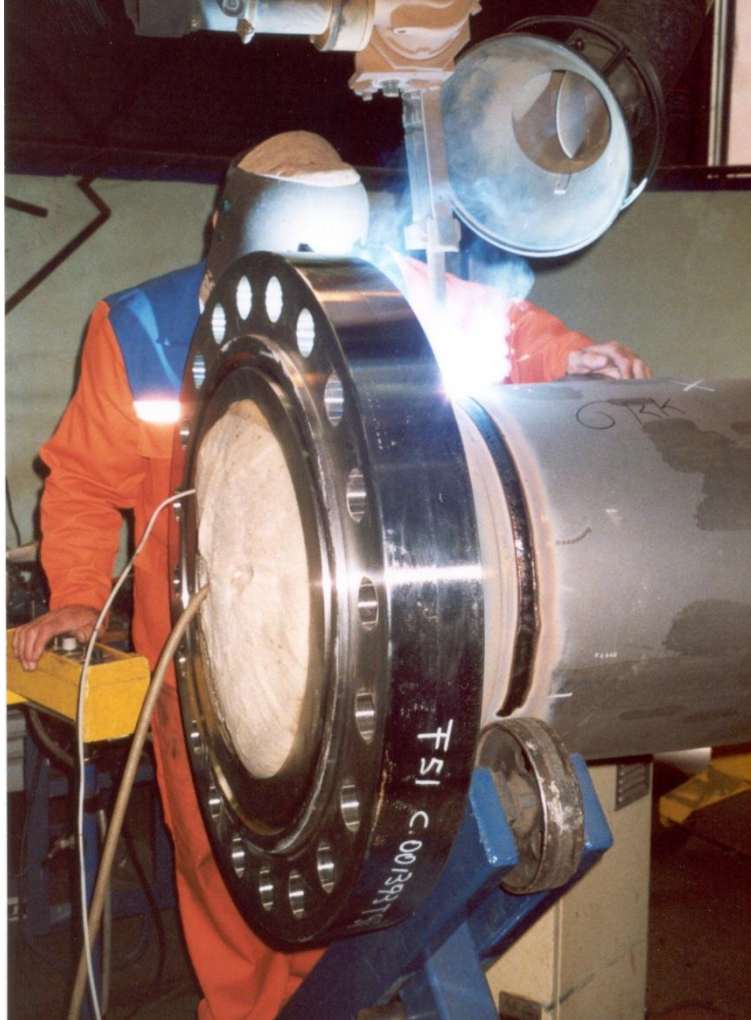
Spatter and embedded slag short arc



Embedded slag spray arc

Avesta 2205 + Avesta FCW-2D 2205

Pipeline oil&gas NAM



voestalpine Böhler Welding

voestalpine

ONE STEP AHEAD.

Slag shielded arc welding

Flux cored arc welding FCAW, $t > 5$ mm

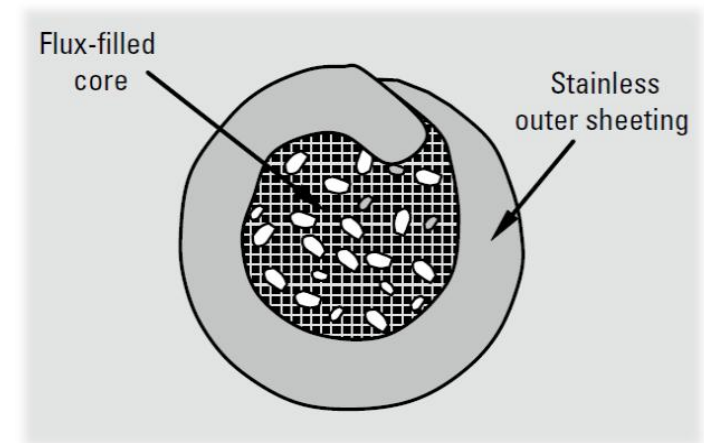
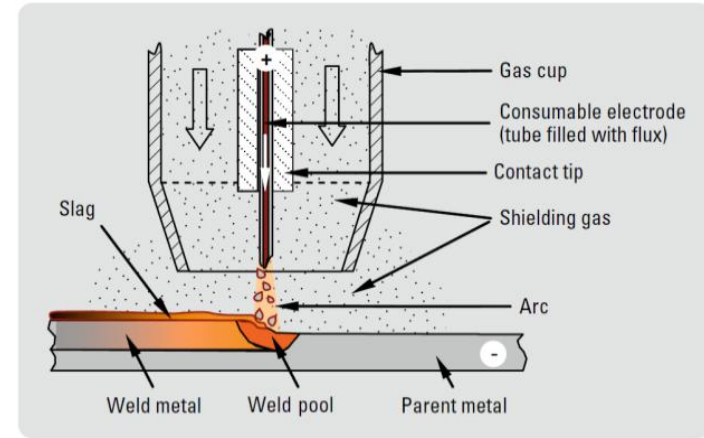
DC+ with normal GMAW machines (4 feeding rolls)

Suitable for prefabrication and onsite welding

Single side welding against ceramic backing

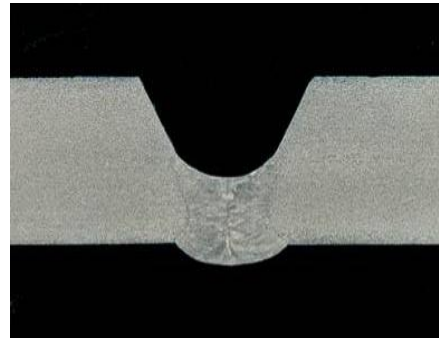
Horizontal and vertical wall position wires

Good positional weldability



-PW

Slag shielded methods give lower impact toughness



Welding with duplex flux-cored wire

Compared to solid wire GMAW – MIG / MAG

Increased productivity and decreased total welding costs

Good side-wall fusion

Wide arc provides uniform, deep penetration

Reduces risk of weld defects (lack-of-fusion)

Less risk of spatter and porosity

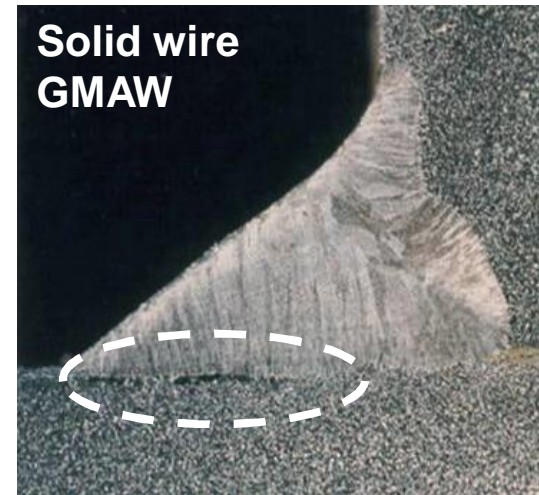
Shielding gas – Ar + 18-25% CO₂

Low shielding gas costs

Good slag removal with suitable welding parameters

Slag-shielded methods give lower impact toughness

Slag removal needed



Change method for improved productivity

Comparison of weld length for fillet welds

Throat thickness 3 mm, welding time 1 min



Flux-cored wire
Ø 1.2 mm

Solid wire
Ø 1.0 mm

Covered
electrode
Ø 3.2 mm

FCAW

GMAW / MAG

SMAW / MMA

References

[Avesta FCW 2507/P100-PW](#)

[Avesta FCW 2507/P100-PW NOR](#)

Companies in France, Germany, Finland, Holland, Poland, UK, Denmark & Spain

Welding duplex and superduplex stainless steel

Repair welding in foundries (filling pores after casting)

Shaft seal and bearing systems for marine industries

Cladding of separators for water sludge, pulp and paper, milk, etc.

Offshore tubes

Water pumps

Pressure vessel – oil treatment & degassing



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ONE STEP AHEAD.

Seawater pumps, Spain

Avesta FCW 2507/P100-PW

Duplex and superduplex stainless steel

Avesta FCW 2507/P100-PW for improved slag removal



Pressure vessel in Uranus 52N+

Success story – Avesta FCW 2507/P100-PW

French fabricator

Moroccan end customer

Welding of pressure vessel in Uranus 52N+

1100 kg Avesta FCW 2507/P100-PW

Chemical industry segment

Phosphoric acid mixer

No specific technical requirements



Flux-cored wires duplex (pure weld metal)

EN TZ 22 9 3 N L R M/C 3 / 1

AWS E 2209 T0-4 (1) / T1-4 (1)

Designation	C	Mn	Cr	Ni	Mo	N	Rp _{0.2}	Rm	A ₅	Impact toughness, J	
							MPa	MPa	%	+20°C	Low temp.
FCW-2D 2205 CN 22/9 N-FD	0.03	0.8	22.7	9.0	3.2	0.13	600	800	27	60	40 (-40°C)
FCW 2205-PW CN 22/9 PW-FD	0.03	0.9	22.7	9.0	3.2	0.13	600	800	27	80	55 (-40°C)

Flux-cored wires superduplex (pure weld metal)

EN TZ 25 9 4 N L P M21 2

AWS E 2594 T1-4

Designation	C	Mn	Cr	Ni	Mo	N	Rp _{0.2}	Rm	A ₅	Impact toughness, J	
							MPa	MPa	%	+20°C	Low temp.
FCW 2507/P100-PW CN 25/9 PW-FD	0.03	0.9	25.3	9.8	3.7	0.23	670	890	26	> 60	34 (-40°C)
FCW 2507/P100-PW NOR	0.03	0.9	25.3	9.8	3.7	0.23	670	890	26	> 60	45 (-50°C)

Pitting corrosion resistance ASTM G48

Pickled samples, test duration 24 h

Corrosion test results CN 22/9 PW-FD Ø1.2 mm

Base material 16 mm EN 1.4462 / UNS S32205, PF (3G), Ar +18% CO₂

Position	Test temperature	Test result (weight loss)
PA	22°C	Pass (0.013 g/m ²)

Corrosion test results CN 25/9 PW-FD Ø1.2 mm

Base material 16 mm EN 1.4410 / UNS S32750, Ar +18% CO₂

V-joints welded against ceramic backing

Position	Test temperature	Test result (weight loss)
PA	40°C	Pass (1.45 g/m ²)
PF	40°C	Pass (0.95 g/m ²)

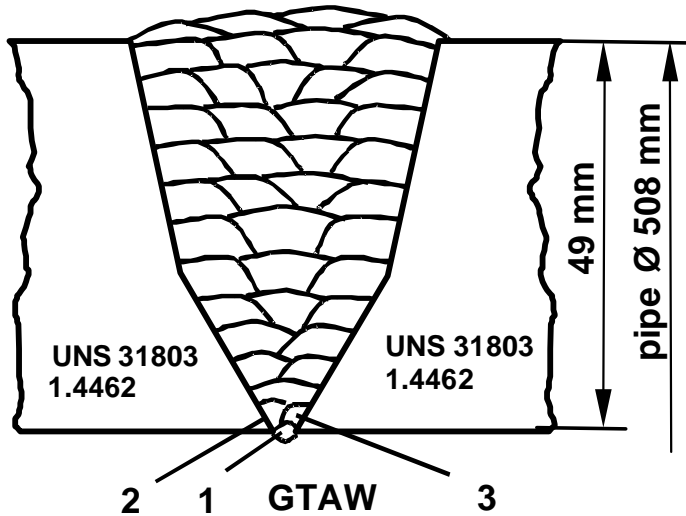
Threshold value pass/fail 4 g/m²

Pipe welded with CN 22/9 PW-FD Ø1.2 mm

Base material 49 mm EN 1.4462, root TIG welded with CN 22/9 N-IG

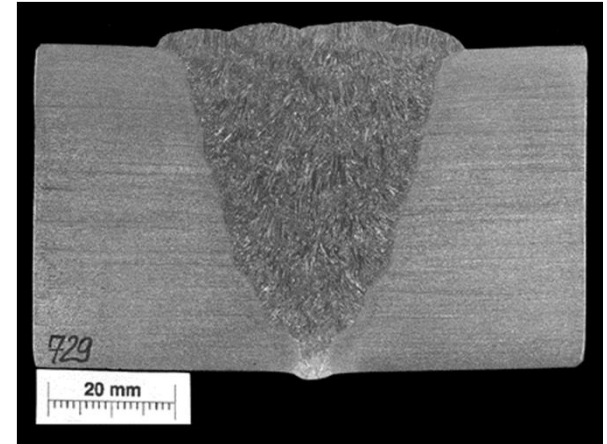
Welding position: 5G (PF), Shielding gas: Ar + 20% CO₂

Interpass temperature: 180°C, Preheating: ~100°C

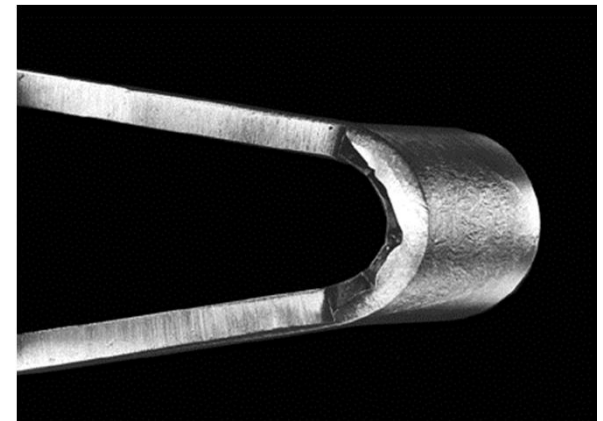


EN 875 10 x 10 mm

Location	Temp.	Impact [J]
WM	+20°C	64 61, 65
WM	-46°C	49, 50, 48



EN 910 bend test accepted
50 x 10 mm, 30 mm mandrel, 180° bend angle



Mechanical properties

AVESTA FCW 2507/P100-PW NOR

Base material – 15 mm EN 1.4410, UNS S32750

V-joint, PF position – measured values (free shrinkage)

Ar + 18% CO₂ as shielding gas

Tensile test				Impact toughness (ISO-V)		
Rp _{0.2} , MPa	Rm, MPa	A ₅ , %	Fracture	+20°C, J	-20°C, J	-46°C, J
706	844	28	Base metal	52, 56, 63	51, 51, 52	40, 49, 44

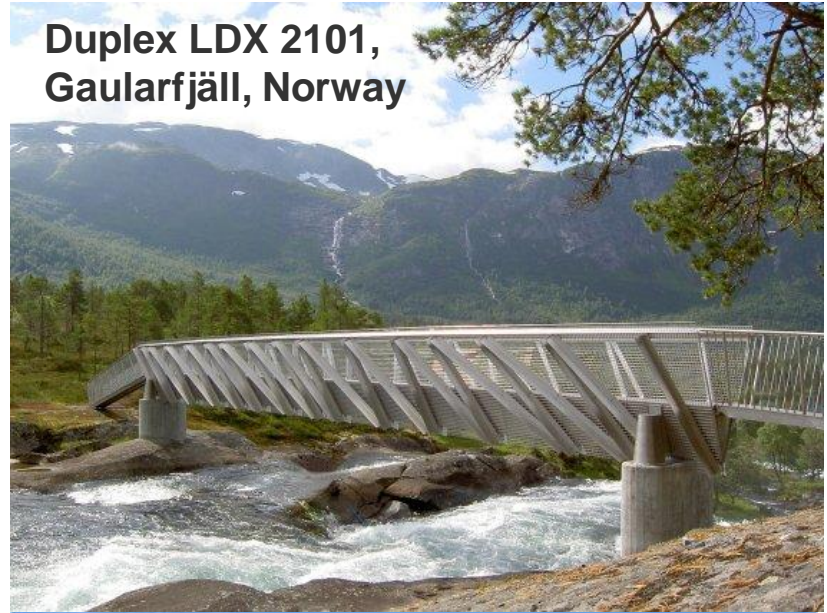
Type	Mandrel Ø, mm	Bend angle	Result
Side bend test	4 × t	180°	No cracks

Bridges made of lean duplex

Avesta FCW LDX 2101-PW, 2304-PW applications



2304, Spain



Duplex LDX 2101,
Gaularfjäll, Norway



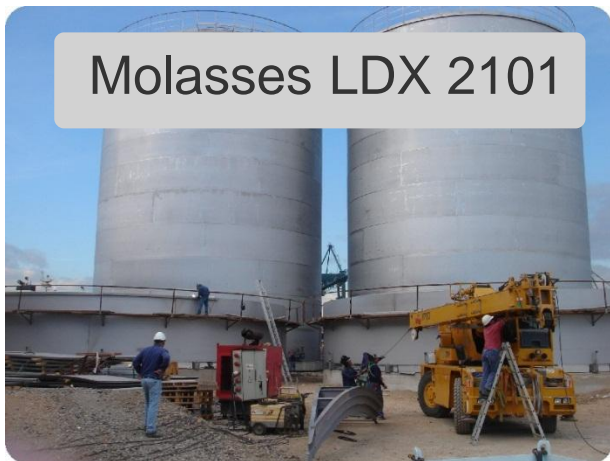
Siena, Toscana, Italy
LDX 2101 (1.4162)



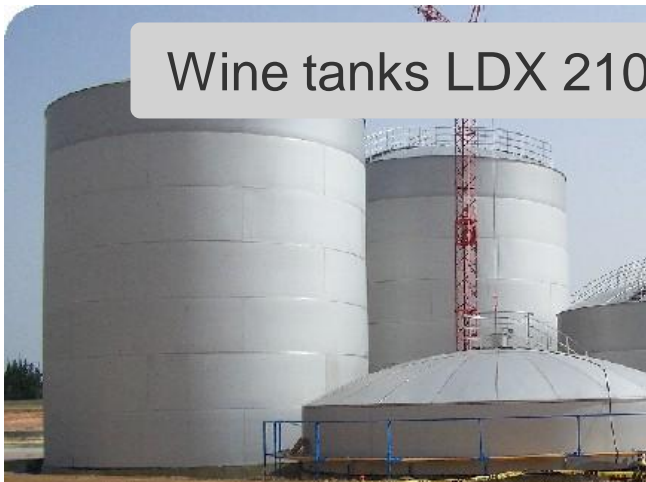
Duplex 2304, Holyhead, UK

Storage tanks welded with FCW

Molasses LDX 2101



Wine tanks LDX 2101 & 2304

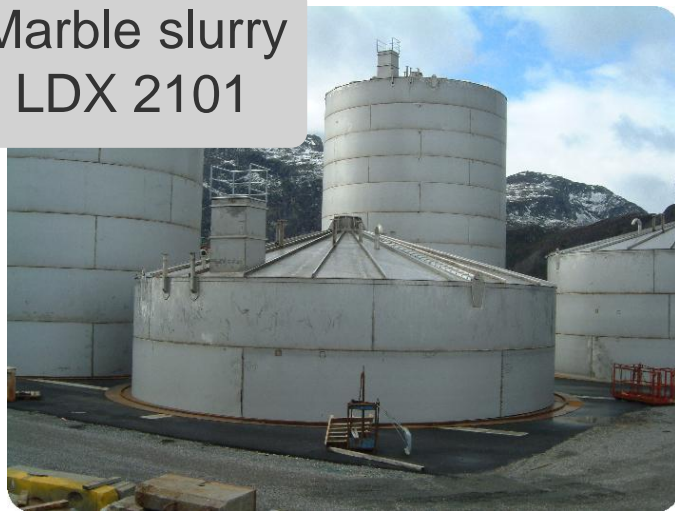


Bio fuel –
2304 + LDX 2101

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ONE STEP AHEAD.

Marble slurry
LDX 2101



Zinc leaching – 2507



Largest pulp digester worldwide

Veracel pulp & paper plant, Brazil (Stora + Aracruz)

Fabricator: Montcalm, Engineering: Andritz

Filler metals:

- 4 500 kg of CN 22/9 N PW-FD
- 1 200 kg of FOX CN 22/9 N
- 700 kg of CN 22/9 N-IG
- 450 kg of CN 23/12 PW-FD
- 650 kg of EAS 2 PW-FD
- 600 kg of EAS 4 PW-FD
- 9 000 kg of other stainless steel coated electrodes, rods and solid wires
- 15 000 kg of carbon steel coated electrodes, rods, flux cored and solid wire

Base metal: Duplex stainless steel UNS S31803



- Welded with: Avesta FCW 2205-PW
- Diameter: 0.045" (1.2 mm)
- Height: 184 ft / 56 m, dia. 34.8 ft / 10.6 m
- Wall thickness: 1.3-2.17" (33-55 mm)
- Horizontal 2G, vertical 3G
- acc. to ASTM A 923 B

Some lean duplex pulp & paper applications

Avesta FCW LDX 2101-PW

TCF bleaching – hydrogen peroxide



LDX 2101[®], Smurfit Kappa, Sweden

Blow tank – LDX 2101, Sweden



Digesters



Continuous, 220



Sulphite
2205, NA



Super Batch, 2205
Thailand



2205, Jiang Lin, China



2205, Veracel, Brazil



2205, Botnia Mill, Uruguay

Heavy transport road tankers

Avesta FCW LDX 2101-PW



LNG tankers outer hull made of LDX 2101, Spain
Improved quality, cost-efficiency and reduced weight



Properties all weld metal

Avesta 2205 grades – mechanical properties, all weld metal

		Tensile strength					Impact toughness [J]			Hardness	
Type	Name	Rp _{0.2} [MPa]	Rm [MPa]	Rm [MPa]	A ₅ [%]	A ₅ [%]	20°C	-40°C	-50°C	Hv10	
SMAW	2205 Bas	660	830	690	26	20	115	75	55	270	290
SMAW	2205-2D	640	825	690	26	20	55	40	-	280	290
SMAW	2205-3D	610	800	690	25	20	55	40	-	280	290
SMAW	2205-4D	630	820	690	25	20	45	35	-	280	290
SMAW	2205-PW	690	870	690	26	20	55	45	35	280	290
GMAW	2205	570	780	690	30	20	150	115	80	280	290
GTAW	2205	620	800	690	28	20	220	210	200	265	290
SAW	2205*	600	800	690	27	20	100	70	-	275	290
FCAW	FCW-2D 2205	600	800	690	27	20	60	40	-	280	290
FCAW	FCW 2205-PW	600	800	690	27	20	80	55	-	280	290

Properties – Welding consumables

Typical weldment properties

Steel grade	ASTM	EN	Welding method	Pitting corrosion ¹ CPT (°C)	Weldment mechanical properties (typical)		
					Rm (MPa)	Impact (J)	
						+20°C	-40°C
LDX 2101	S32101	1.4162	GMAW	> 6 ²	725	150	110
			FCAW	> 6 ²	725	63	45
2304	S32304	1.4362	GMAW	> 10	640	150	110
			FCAW	> 10	700	50	40 (-20°C)
2205	S32205	1.4462	GMAW	> 22	780	150	110
			FCAW	> 25	770	60	40
2507	S32750	1.4410	GMAW	> 35	850	140	50 (-46°C)
			FCAW	> 35	890	60	45

Weld repair of cast in foundries – FCAW

Success story at AMPO Valves Idiazabal, Spain

- ▶ Replacing GMAW to avoid porosity
- ▶ PW wires - do not have to turn large pieces in best position
- ▶ High productivity



Customer testing – repair welding in foundry

FCAW with Ø1.2 mm FCW 2507/P100-PW NOR

Delivers much material to offshore industry

Have struggled with procedure testing with other products

32.5 V, 237-243 A, 7-9.5 mm/s welding speed

Solution annealing 1120°C for 2.5 min/mm + water quenching

Impact toughness at -46°C: 76, 79, 75 J

Weld metal ferrite content: 45 ± 5%

ASTM G48 Method A approved at 50°C / 24 h

Some possible material combinations

- Mild steels
- Fine grained steels
- High temperature steels
- Low temperature steels
- Martensitic/Ferritic Cr-steels
- Austenitic CrNi(Mo)-steels
- Duplex steel
- Nickel-base alloys



- Martensitic Cr-steels
- Ferritic Cr-steels
- Sort martensitic CrNi-steels
- Austenitic CrNi(Mo)-steels
- Duplex steel
- Nickel-base alloys

Dissimilar welding

*P12 = Ni Cr 22 Mo 9 Nb, Ni Cr Mo-3

*P16 = Ni Cr 23 Mo 16, Ni Cr Mo-13

Grade	LDX 2101	2304	2205	2507	304	316	254 SMO "6Mo"	Carbon Steel
LDX 2101	23 7 N L 22 9 3 N L	23 7 N L 22 9 3 N L	22 9 3 N L	25 9 3 Cu N L	23 7 N L 23 12 2 L 23 12 L	23 7 N L 23 12 2 L	P12* P16*	23 7 N L 23 12 2 L 23 12 L
2304	23 7 N L 22 9 3 N L	23 7 N L 22 9 3 N L	22 9 3 N L	25 9 3 Cu N L	23 7 N L 23 12 2 L 23 12 L	23 7 N L 23 12 2 L	P12* P16*	23 7 N L 23 12 2 L 23 12 L
2205	22 9 3 N L 23 7 N L	22 9 3 N L	22 9 3 N L	25 9 3 Cu N L	22 9 3 N L 23 12 2 L 23 12 L	22 9 3 N L 23 12 2 L	P12* P16*	22 9 3 N L 23 12 2 L 23 12 L
2507	25 9 3 Cu N L	25 9 3 Cu N L	25 9 3 Cu N L	25 9 3 Cu N L	25 9 3 Cu N L 23 12 2 L 23 12 L	25 9 3 Cu N L 23 12 2 L	P12* P16*	25 9 3 Cu N L 23 12 2 L 23 12 L

Dissimilar welding

Testing in accordance with BS 4515-2 + client specification

Forging grade A182 F53 to pipe A790 UNS S32760

GTAW weld root

Avesta FCAW 2507/P100-PW NOR

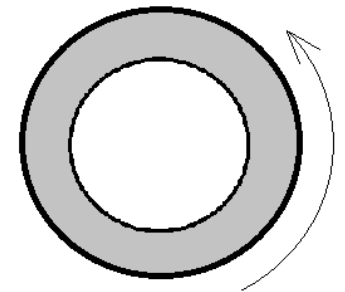
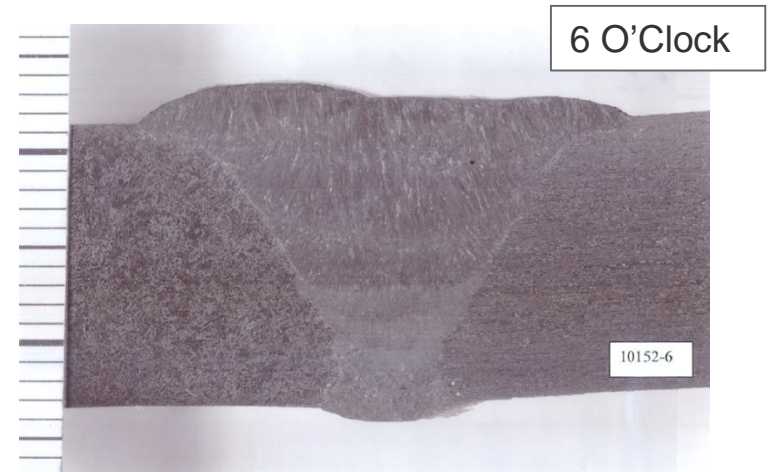
5G (PF) position

All testing approved:

Cross-tensile tests, requirement $R_m \geq 750$

Hardness HV 10, requirement $HV_{10} \leq 350$

Impact toughness Charpy KV, as info at -40°C
(measured mean value 88 J)



Welding duplex steels of similar composition

Steel grades	Böhler	Avesta
LDX 2101, S32101, 1.4162, S32001, 19D	CN 24/9 or CN 22/9	LDX 2101 or 2304 or 2205
ASTM 329	CN 22/9	2205
AL 2003 (UNS 32003)	CN 22/9	2205
3RE60 (S31500)	CN 22/9	3RE60 or 2205
1.4363, S32304, URANUS 35N, SAF 2304	CN 24/9 or CN 22/9	2304 or 2205
1.4662, LDX 2404, S82441	CN 22/9, CN 25/9	2205, 2404, 2507
1.4462, S32205, SAF 2205, Uranus 45N, Remanit 4462, 1903SC, AF22, CS22, Falc 223, SM 22Cr, NKCr22	CN 22/9	2205
1.4410, S32750, SAF 2507, 1.4510, Zeron 100, DP-3W, S32760, Uranus 52M+	CN 25/9 (CuT)	2507/P100

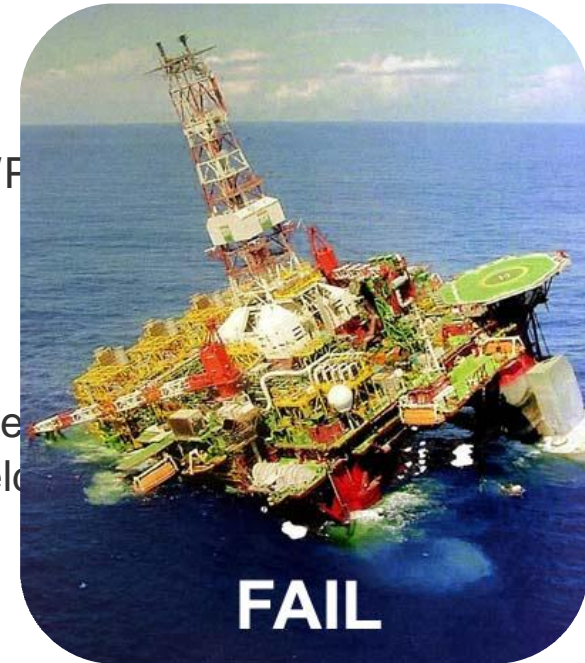
How to avoid unexpected phenomena?

Use QA system for welding in EN ISO 3834-(1-3)

EN-ISO 15614 – establishing welding procedure

- preliminary welding procedure specification (pWPS)
- welding procedure qualification record (WPQR)
- welding procedure specification (WPS)

Based on test welding (pWPS) and results from testing (WPQR) of specific weld, responsible welding engineer creates approved WPS that welders shall follow in field



Further train welders and operators on how to weld involved grades, necessity of post-weld cleaning for corrosion resistance and how they can minimize needed pickling time by handling material properly

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ONE STEP AHEAD.

Main challenges when welding superduplex

From voestalpine Böhler Welding's point of view

Risk of sigma phase formation (intermetallics)

- Negative for corrosion resistance and impact toughness
- Limits heat input and interpass temperature

Corrosion testing ASTM G48

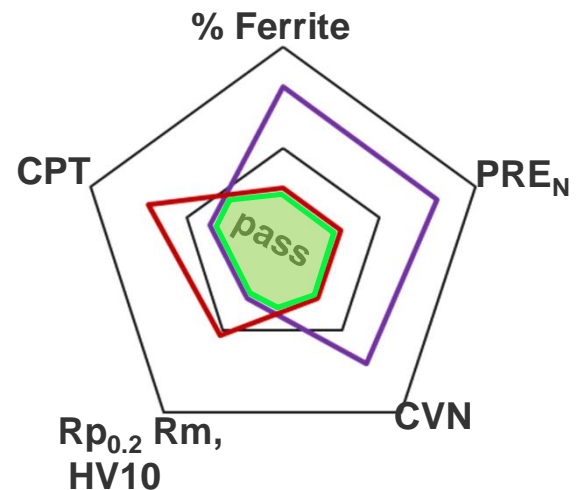
- Pickling required
- Specified test temperature too high
- Pure argon often used as backing gas

Impact toughness

- More productive slag-shielded methods
- High austenite content good, but often limited to 35–65%

Conservative specifications limit use of e.g. some methods and gases

Increasingly conservative specifications



Main challenges when welding superduplex

From Böhler Welding Group's point of view

Corrosion testing of superduplex (ASTM G48)

- Pure argon often used
- Best backing gas not always allowed

Impact toughness

- More productive slag-shielded methods
- High austenite content good, but often limited to 35-65%

Specifications limits use of

- FCAW (e.g. Total, Petrobras)
- Nitrogen in backing gas (e.g. Total)
- Hydrogen in nitrogen-based backing gas (e.g. Shell)

Thank you for your attention!

**A special
view for
special
steels!**



Thank you!

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